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by

Keto Soosaar Roland Grin

Martin Furey Joseph Hamilton

April 1975

This report covers research conducted between January I, 1974 and September I, 1974



The Charles Stark Draper Laboratory, Inc.

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The publication of this report does not constitute approval by the National Aeronautics and Space Administration of the findings on conclusions contained herein. It is published only for the exchange and stimulation of ideas.

Structural Evaluation of Candidate Designs for the Large Space Telescope Primary Mirror

by

Roland Grin Keto Soosaar

and

Martin Furey Joseph Hamilton

ABSTRACT

Structural performance analyses have been conducted on two candidate designs for the NASA Large Space Telescope three-meter mirror. In a NASA Phase "B" competition the Itek Corp. and the Perkin-Elmer Corp. have each proposed a mirror using separate design configurations and different substrate materials. The mirror designs and the finite-element models used in the analyses evaluation are described. The results of the structural analyses for several different types of loading are presented in tabular and graphic forms.

Several additional analyses are also reported herein. These include the evaluation of a new mirror design concept proposed by the Boeing Co., a study of the global effects of local cell plate deflections, and an investigation of the fracture mechanics problems likely to occur with Cervit and ULE. Also, flexibility matrices were obtained for the Itek and Perkin-Elmer mirrors to be used in active figure control studies.

Summary, conclusions and recommendations complete the report.

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Chapter 1

INTRODUCTION

This report documents structural analyses that were performed to help evaluate various "Phase B" designs for the primary mirror of the NASA Large Space Telescope.

Chapters 2 and 3 of the report discuss the two competing mirror designs, both of which were of lightweighted construction. The Itek Corp. design utilizes Owens-Illinois CERVIT material with a core lightweighted into hexagonally-shaped cells and a circumferential edge band. The Perkin-Elmer Corp. design uses Corning ULE, and is assembled with a core of square cells and a circumferential edge band. Both mirrors are compared under various inertial (Chapter 2) and thermal (Chapter 3) loads.

Chapters 4 and 5 contain additional miscellaneous investigations. Found here is the analysis of a CERVIT mirror to be constructed using an alternate simpler light-weighting technique proposed by the Boeing Co. Then a study is reported that was conducted to evaluate the additional effect of local cell deflections on the total mirror performance under 1G transversely applied. Finally some preliminary investigations are performed on the fracture mechanics problems associated with the use of CERVIT and ULE.

As an aid in the investigation of the active mirror figure control concept, unit loads representing actuators moving parallel to the optical axis are placed at a number of positions on the back surface of the mirror. The resulting deflection data is then used to generate the control matrices. This is discussed in Chapter 5 and the flexibility matrices are listed in Appendix B.

Chapter 2

INERTIAL LOAD EFFECTS ON THE ITEK AND PERKIN-ELMER PRIMARY MIRRORS

2.1 Description of Mirror Designs

The properties of the Itek and Perkin-Elmer primary mirrors are listed in Table 2.1. Each mirror is made of a "glassy" low thermal expansion material and is of a composite sandwich construction. The Itek mirror is machined from a solid blank of CERVIT and has a core lightweighted with hexagonally-shaped cells. It has a circumferential edge band at both the inside and outside diameters.

The Perkin-Elmer mirror is assembled from ULE plates fused together with a lightweighted core of square-shaped cells, and continuous circumferential and internal edge bands. Both mirrors are held at their outside edge at supports 120° apart which allow expansion in the radial direction. The Itek mirror is supported at a cylindrical trunnion at the mid-height of the outside edge band in a solid area and the Perkin-Elmer mirror is supported axially at the intersection of the back plate with the outside edge and tangentially at mid-height. Both support areas are considerably reinforced.

2.2 Inertial Loads

1G loads are applied individually in the direction of each of the three principal axes; that is, parallel to the optical axis (-Z direction) and along the X and Y axes which are parallel to the plane of the mirror. While all

PROPERTIES	ITEK	PERKIN-ELMER
Outside Diameter	3.05m (120 in.)	3.05m (120 in.)
Inside Hole Diameter	.813m (32 in.)	.635m (25 in.)
Spherical Radius of Curvature	14.4m (566.9 in.)	14.68m (578 in.)
Radial Thickness	.381m (15 in.)	.381m (15 in.)
Cell Shape	Hexagonal	Square
Cell Pitch	.122m (4.8 in.)	.102m (4.0 in.)
Top Plate Thickness	2.54cm (1.0 in.)	3.81cm (1.5 in.)
Bottom Plate Thickness	3.02cm (1.19 in.)	3.81cm (1.5 in.)
Bottom Plate Hole Diameter	8.255cm (3.25 in.)	None
Edge Band Thickness	1.016cm (.40 in.)	.635cm (.25 in.)
Cell Wall Thickness	.508cm (.20 in.)	.508cm (.20 in.)
Percent Light Weighting	91.6%	90%
Total Weight Mirror	1847kg (4071#)	1723kg (3800#)
Material Density E (Young's Modulus)	CERVIT 2491 Kg/m ³ (.09 lb/in. ³) 9.24 x 10 ¹⁰ N/m ²)	ULE 2214 Kg/m ³ (.08 lb/in. ³) 6.76 x 10 ¹⁰ N/m ²
_ ,,,	(13.4 x 10 ⁶ PSI)	(9.8 x 10 ⁶ PSI)
Poisson Ratio	. 252	.170
Nominal Temperature Coefficient	.05 cm/cm/°Cx10 ⁻⁶	.03 cm/cm/°Cx10 ⁻⁶
	(.277 x 10 ⁻⁷ in/in/°F)	(.167 x 10 ⁻⁷ in/in/°F)

Table 2.1 Properties of the Itek and Perkin-Elmer Primary Mirrors

three loading directions are important in evaluating dynamic effects, the optical axis direction is most significant in the manufacturing and, hence, the zero-g release problem. The response along the X and Y axes is important in launch evaluation.

2.3 Structural Models

Since the time available to evaluate the competing Phase B designs was limited to about seven weeks, the modeling was necessarily approximate, and the "Trade-off Model, " as described in Ref. 1, had to be used. Within this type, two sizes of finite element models were used. In analyzing for a 1G load parallel to the optical axis (-Z direction) a 60° segment was modeled. Roller supports were provided along the radial edges. In the analysis for the 1G loads perpendicular to the optical axes (X and Y directions) the entire mirror was modeled. The Itek 60° model is shown in Figure 2.1 and the full 360° model in Figure 2.3. The Perkin-Elmer 60° model is shown in Figure 2.2 and the full 360° model is shown in Figure 2.4. The supports at the circumference for the 360^{O} models are shown in Figures 2.5 and 2.6. The mirror lightweighted cores were idealized as a solid continuum and were modeled using isoparametric 3D solid finite elements. The top and bottom plates and circumferential edge bands were modeled using plate elements. ICES-STRUDL II was used for all finite element computations.

2.4 Results of Analyses

2.4.1 1G Load Parallel to The Optical Axis (-Z)

A comparison of the deflections of the Itek versus

^{*} See Bibliography

the Perkin-Elmer mirror under a 1G load parallel to the optical axis is given in Table 2.2. Z-contour deformations of the mirror top surfaces are shown in the Appendix in Figures A-1 and A-2. Maximum stresses at the front and back surfaces of the mirrors are shown in Figures 2.7 and 2.8 for the Itek mirror, and Figures 2.9 and 2.10 for the Perkin-Elmer mirror.

2.4.2 lG Loads in The Lateral (+X and +Y) Directions

The deformations shown in Figures 2.11 and 2.12 for the Itek mirror under 1G loads in the X and the Y directions are primarily rigid body displacements due to deflections in the mounts. The maximum stresses in the front plate of the mirror are shown in Figures 2.13 and 2.14, and in the rear plate in Figures 2.15 and 2.16.

The displacements at the mounts for the Perkin-Elmer mirror under a 1G load in the +X direction and a 1G load in the +Y direction are given in Tables 2.3 and 2.4. The coordinate system and the node numbers are shown in Figure 2.6. The maximum stresses in the front plate of the Perkin-Elmer mirror are given in Figures 2.17 and 2.18, and in the rear plate in Figures 2.19 and 2.20.

2.4.3 Remarks on Units

As all of the mirror drawings and material properties were provided to CSDL in the English system, the finite element modelling was performed using inches and pounds. It later developed that the optical surface displacements were desired in SI units. The results were then converted to that system, although for convenience, most of the summary tables use both sets of units. The "unit" thermal studies were performed with l^OF changes and gradients. These were not converted to ^OC changes since that can be readily performed when the actual temperatures are known, by inserting an additional factor of 1.8.

Designer	Material	Structural Type	Direction of 1G Gravity Load	Maximum Deflection Z-Direction 10 ⁻⁸ M (10 ⁻⁶ in)		
				Δ	Peak to Peak	RMS
ITEK	CERVIT	60 ⁰ Segment equiv- alent solid core	-Z (transverse)	922 (363)	712 (281)	154 (61)
PERKIN-ELMEI	ULE	60 ⁰ Segment equiv- alent solid core	-Z (transverse)	1181 (465)	820 (323)	185 (73)

Comparison of Deflections, Itek Vs. Perkin-Elmer Mirror, 1G Load in -Z Direction

Table 2.2

DISPLACEMENT AT MOUNTS, PERKIN-ELMER MIRROR 1G LOAD IN THE +X DIRECTION

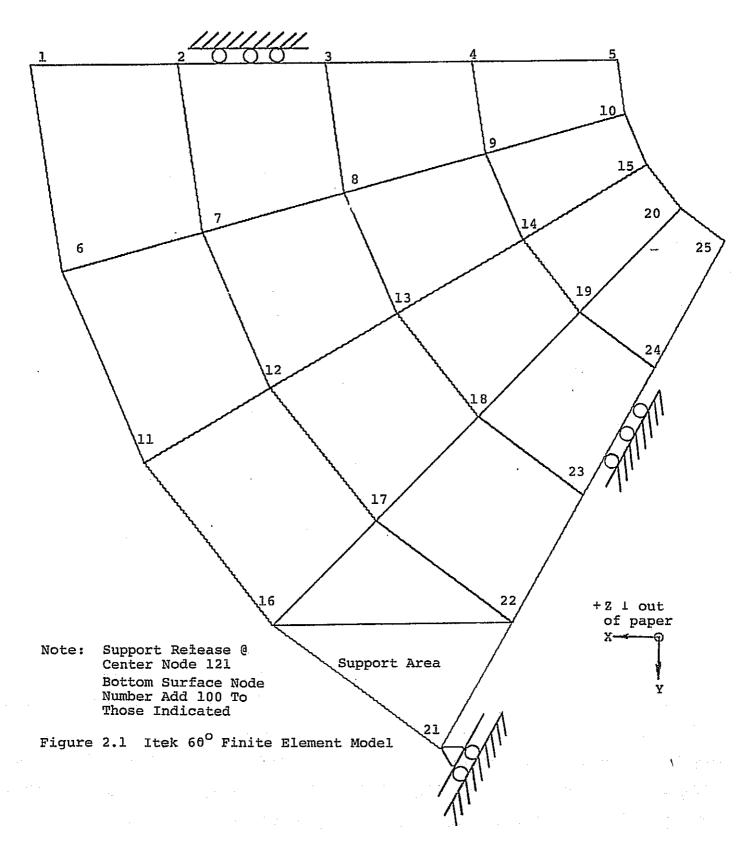
		Displ. x10 ⁻⁸ M (10 ⁻⁶ in)		
N	ode #	ΔΧ	ΔY	ΔZ
	129	+1821 (+717)	+200 (+79)	45.7 (+18)
Axial Mounts	123	+1953 (+769)	-51 (2)	-61 (-24)
Modifics	.126	+1727 (+680)	-20.3 (-8)	+15.2 (+6)
Tangential	121	+1666 (+656)	+200 (+79)	-20.3 (-8)
Mounts	125	+1953 (+769)	0 (0)	-76.2 (-30)
	128	+1653 (+651)	-175 (-69)	+88.9 (+35)

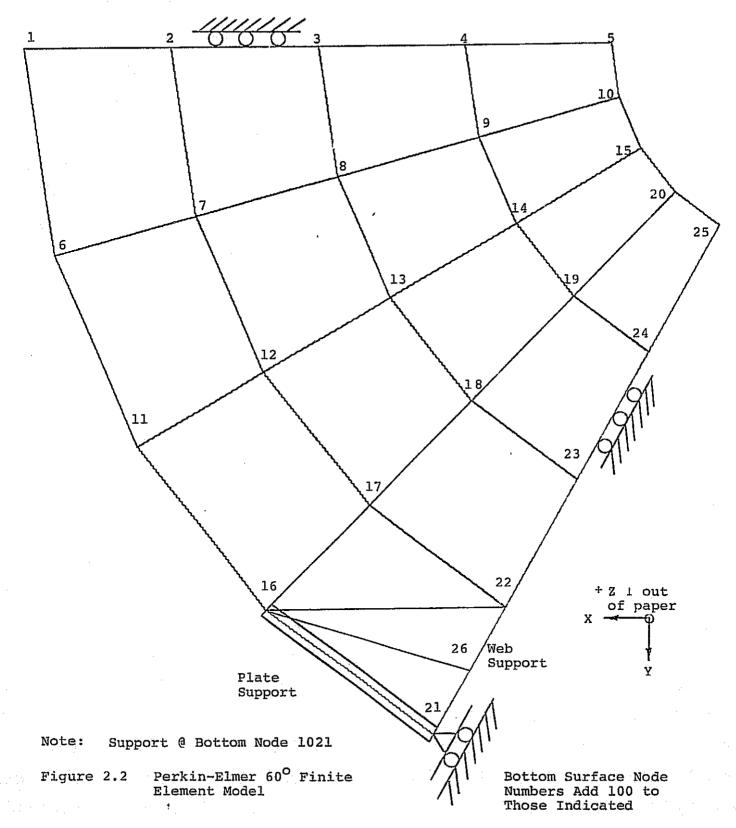
Table 2.3

DISPLACEMENT AT MOUNTS, PERKIN-ELMER MIRROR 1G LOAD IN THE +Y DIRECTION

		Displ. x10 ⁻⁸ M (10 ⁻⁶ in.)		
Node #		ΔΧ	ΔΥ	ΔΖ
Axial Support	129 123 126	+88.9 (+33) -122 (-48) -127 (-50)	+1849 (+728) +1720 (+677) +1950 (+768)	+45.7 (+18) +17.8 (+7) -61 (-24)
Tangential Support	121 125 128	+173 (+68) +5.1 (+2) -175 (-69)	+1849 (+728) +1552 (+611) +1857 (+731)	+99.1 (+39) -58.4 (-23) -35.6 (-14)

Table 2.4





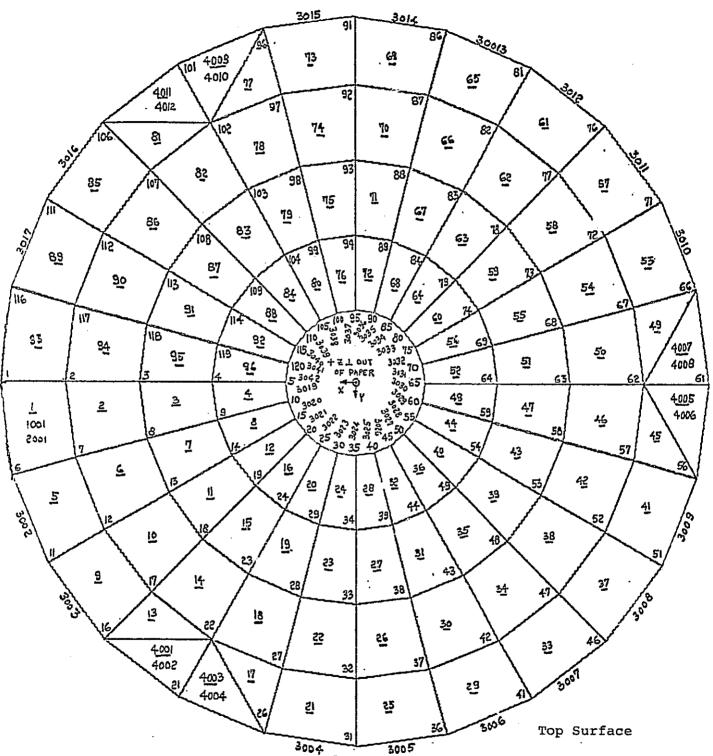


Figure 2.3 Itek 360° Finite Element Model

Bottom Surface Node Numbers ADD 1000 To Those Indicated

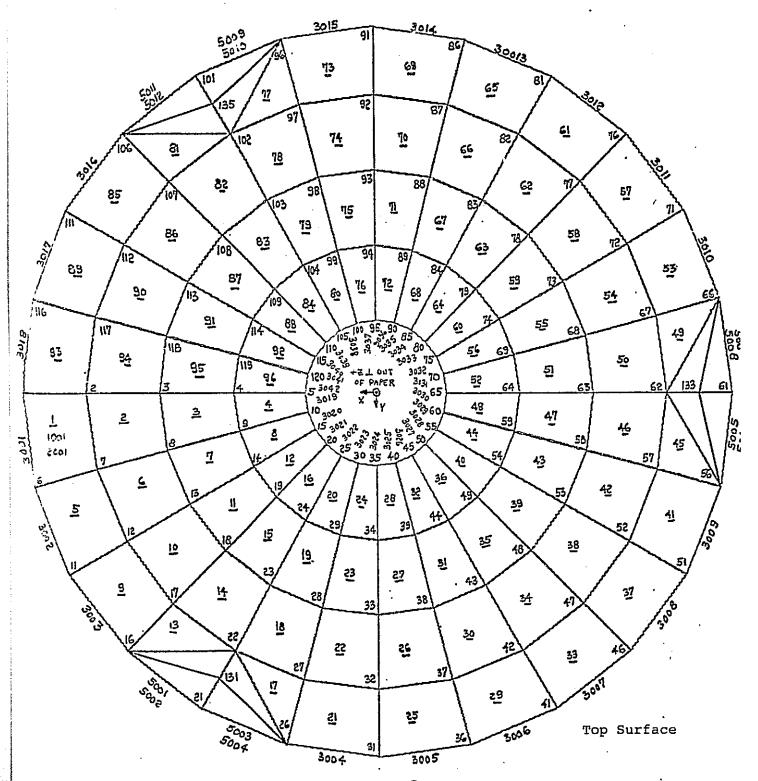
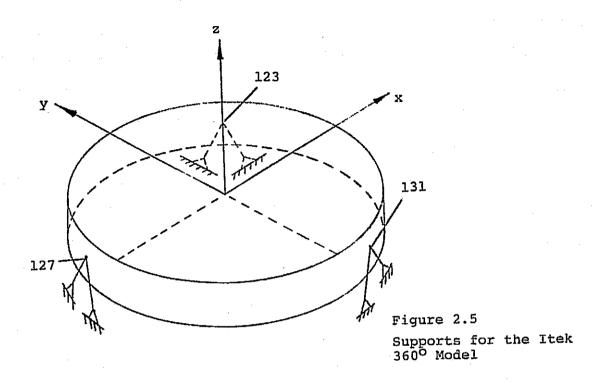
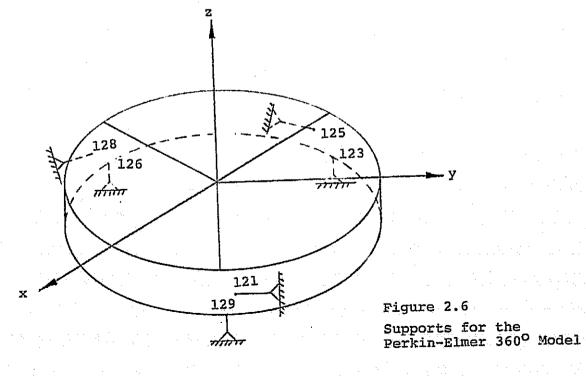


Figure 2.4 Perkin-Elmer 360° Finite Element Model





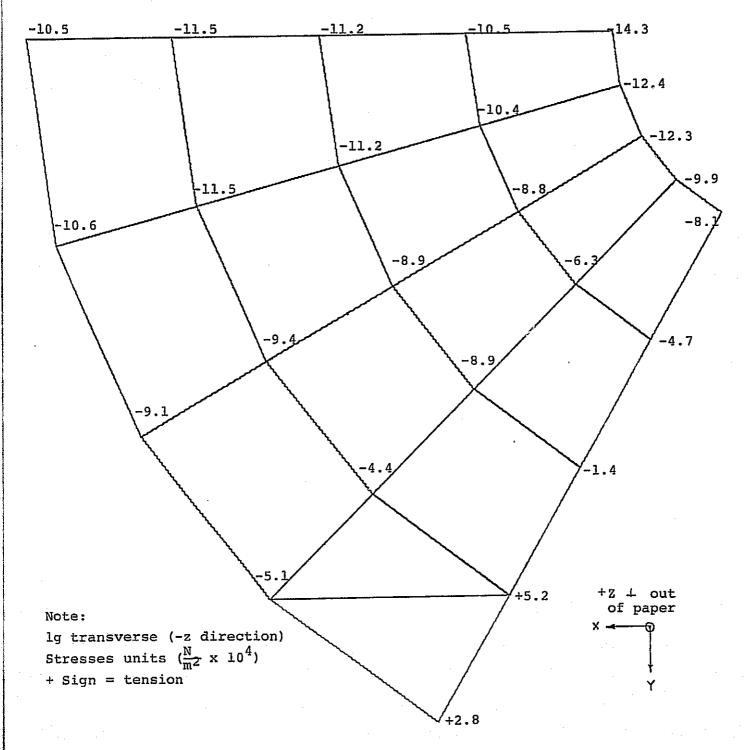


Figure 2.7 Maximum Stresses, Front Plate of Itek Mirror

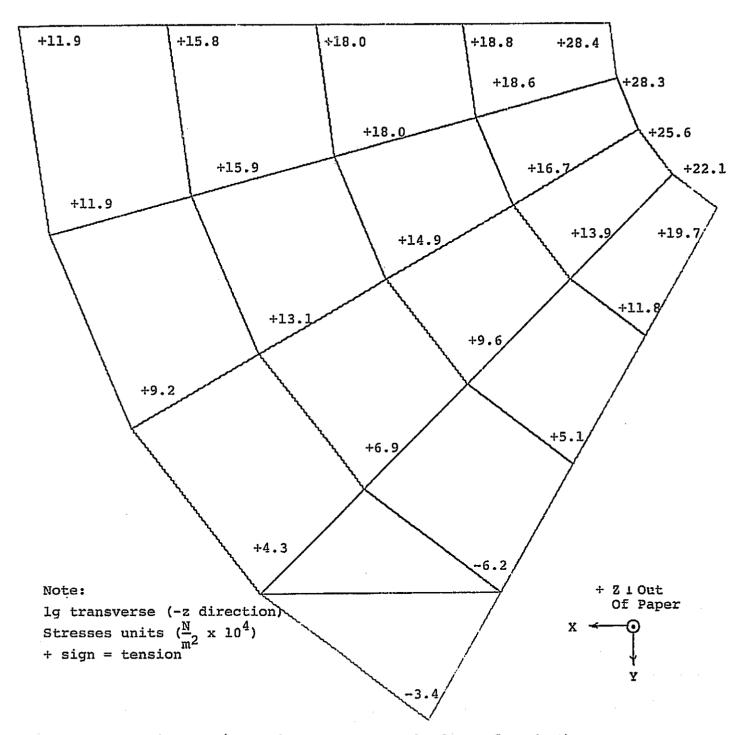


Figure 2.8 Maximum Stress, Back Plate of Itek Mirror

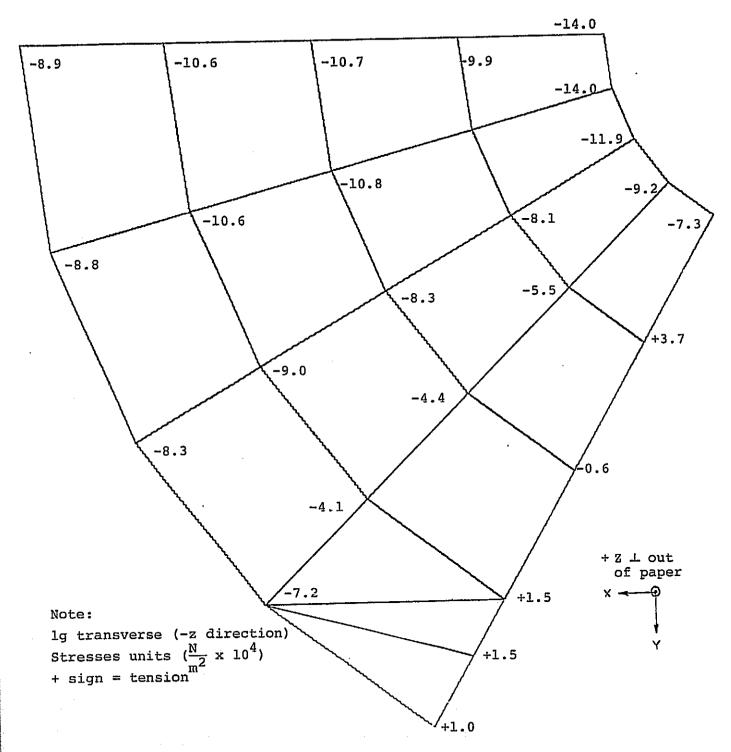


Figure 2.9 Maximum Stresses, Front Plate of Perkin-Elmer Mirror

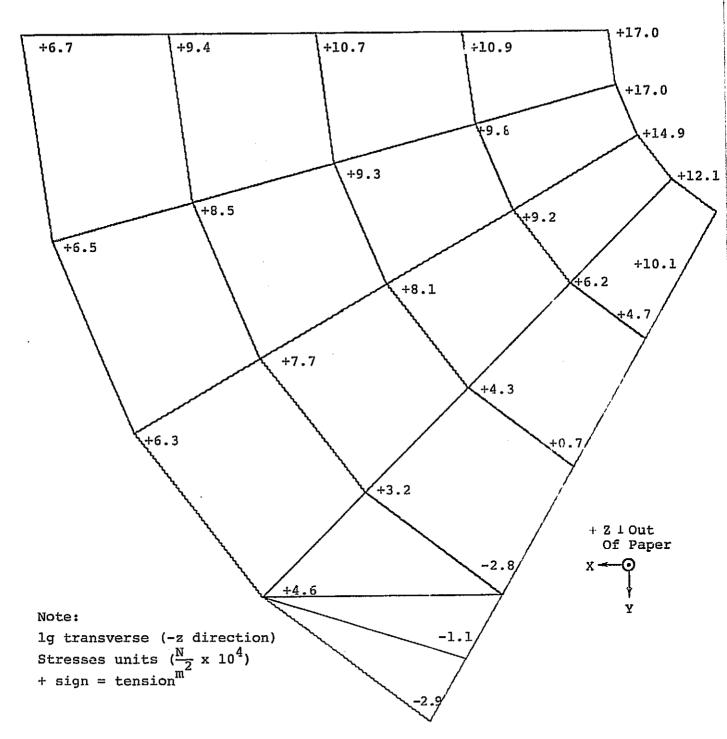


Figure 2.10 Maximum Stresses, Back Plate of Perkin-Elmer Mirror

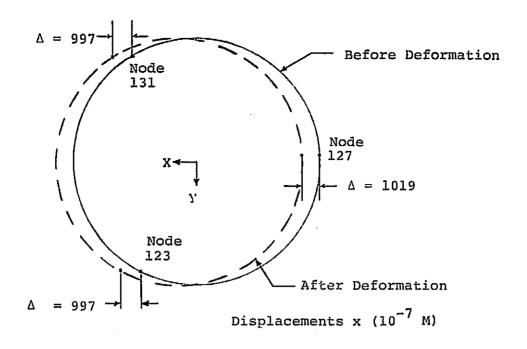


Figure 2.11 Deflection of Itek Mirror, lg Load in X Direction

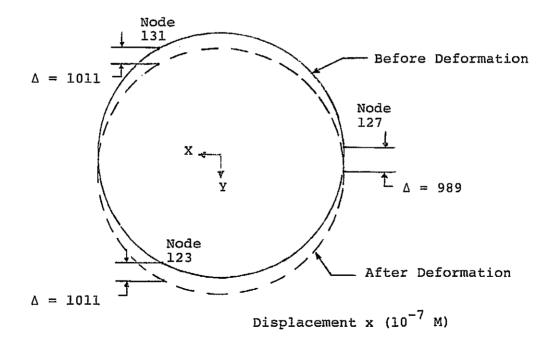


Figure 2.12 Deflection of Itek Mirror, lg Load in Y Direction

Figure 2.13 Stress Front Plate of Itek Mirror, lg Load in x Direction

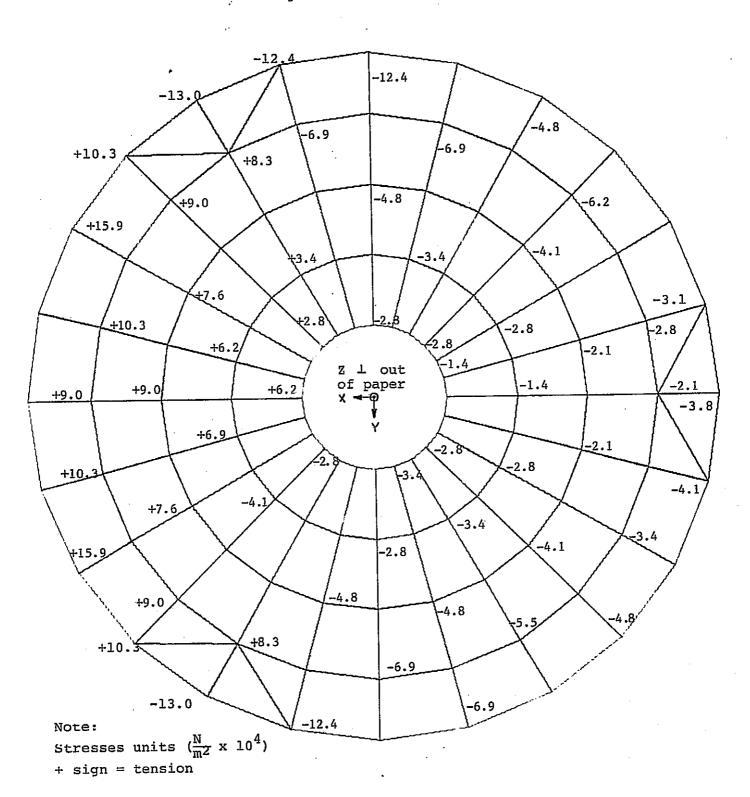


Figure 2.14 Stress Front Plate of Itek Mirror, lg Load in y Direction

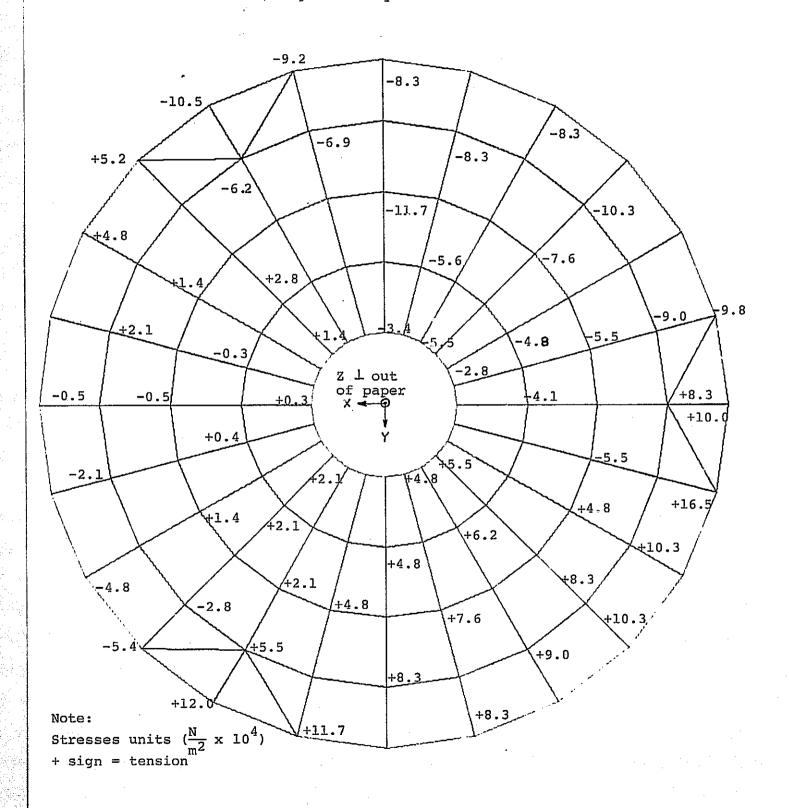


Figure 2.15 Stress Back Plate of Itek Mirror, lq Load in X-Direction

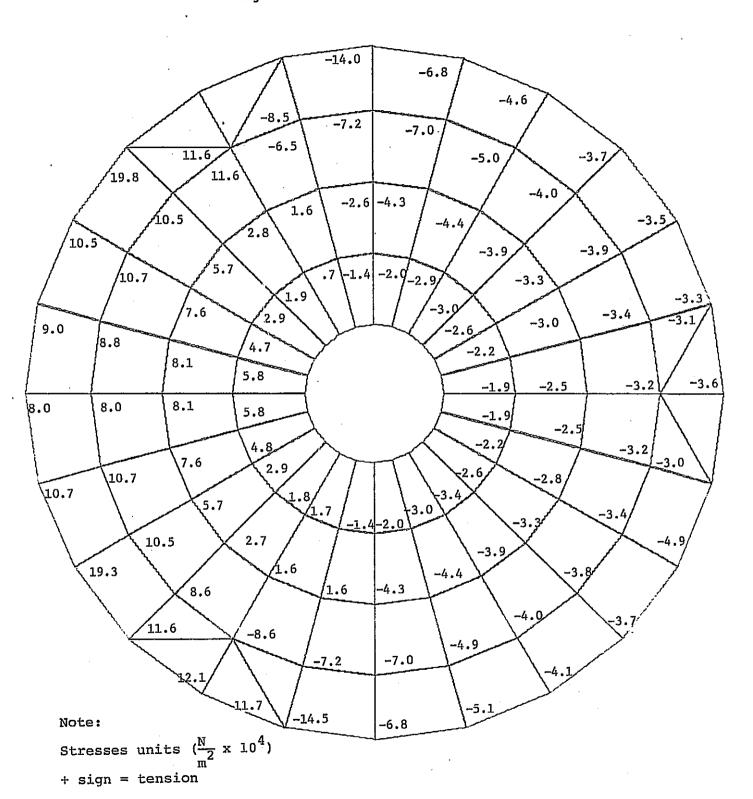


Figure 2.16 Stress Back Plate of Itek Mirror, lq Load in Y Direction

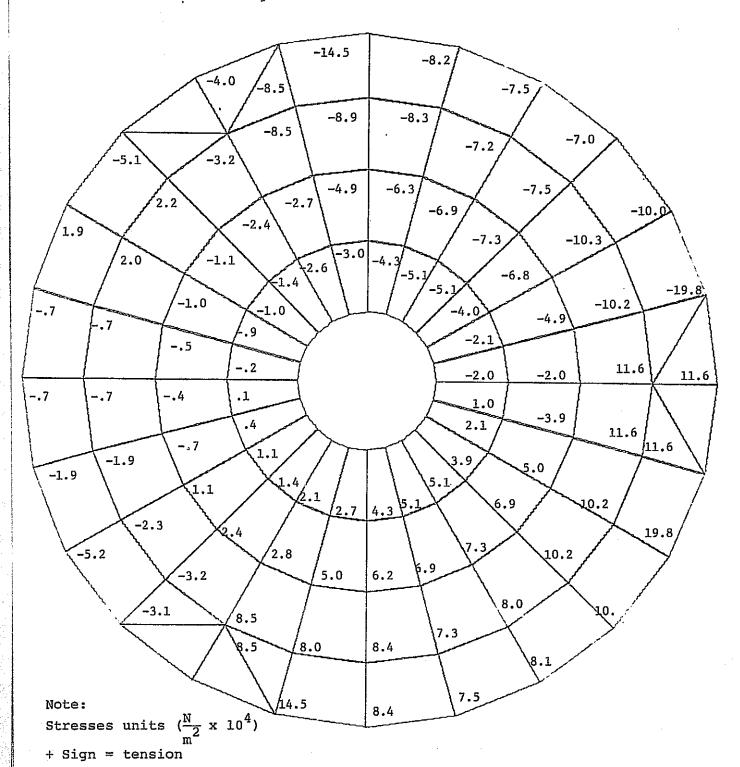


Figure 2.17 Stresses Front Plate of Perkin-Elmer Mirror lg Load in x Direction

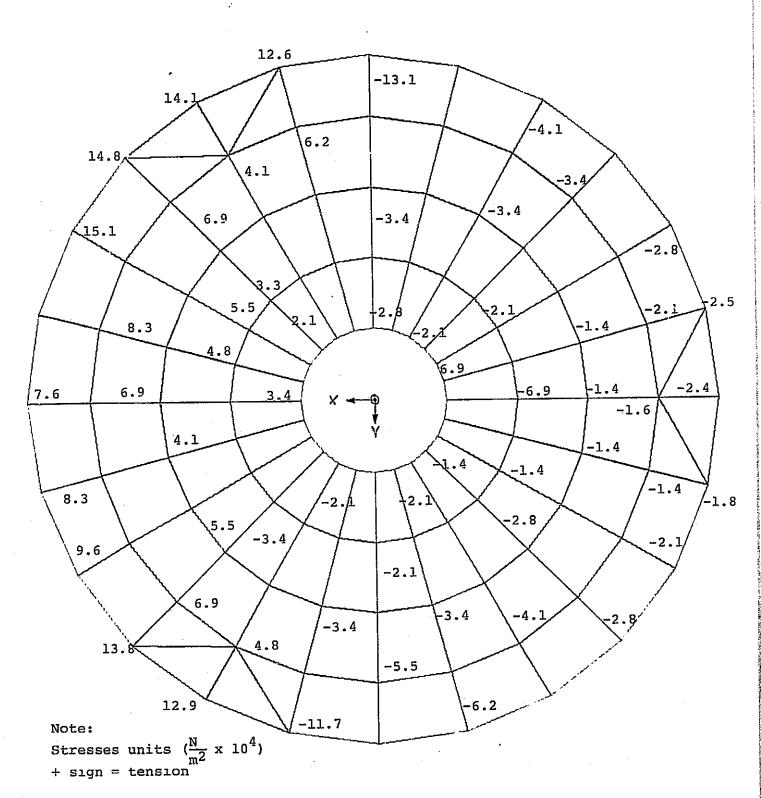


Figure 2.18 Stresses Front Plate of Perkin-Elmer Mirror lg Load in y Direction

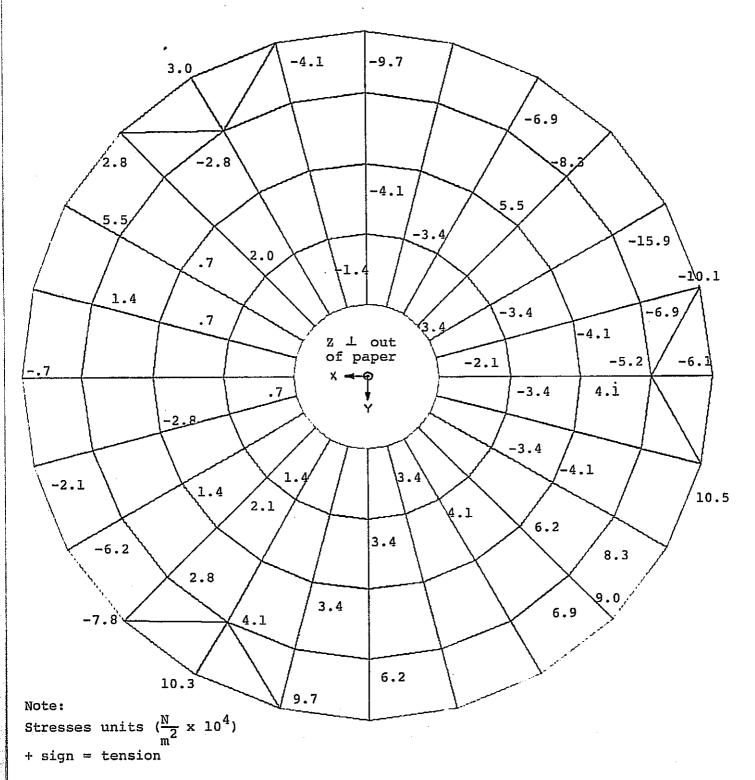
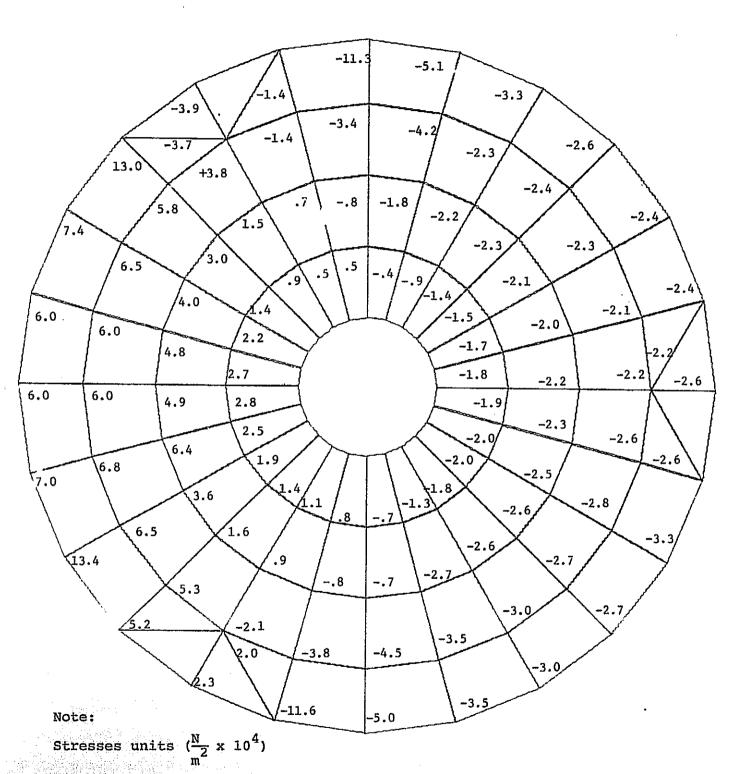


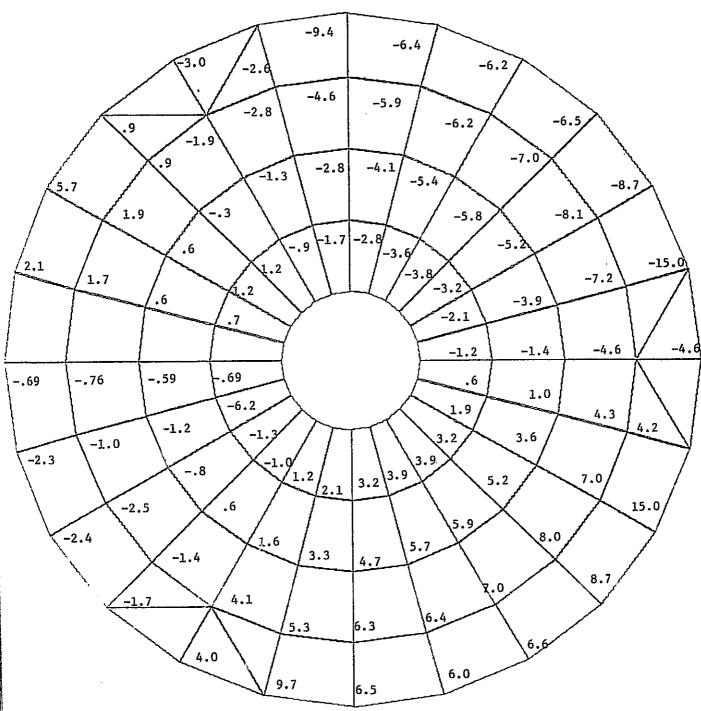
Figure 2.19 Stress Back Plate of the Perkin-Elmer Mirror, lg Load in X Direction



+ sign = tension

Figure 2.20 Stress Back Plate of the Perkin-Elmer Mirror, lg Load in Y Direction

,•



Note:

Stresses units $(\frac{N}{m^2} \times 10^4)$

+ sign = tension

Chapter 3

THERMAL LOAD EFFECTS ON THE ITEK AND PERKIN-ELMER MIRRORS

3.1 Thermal Loads

For the Itek CERVIT design four different sets of thermal expansion coefficients were used. The "nominal" coefficient ($\alpha = .05 \times 10^{-6} \text{M/M/}^{\circ}\text{C.}$) and those obtained at 10°C. , 15°C. and 25°C. for the particular blank available. Three different thermal loadings were imposed: a 1°F. uniform soak, a 1°F. axial gradient and a 1°F. radial gradient. This yielded twelve cases to be investigated.

For the Perkin-Elmer ULE design two sets of thermal expansion coefficients were used. The nominal coefficient ($\alpha = .03 \times 10^{-6} \text{M/M/}^{\circ}\text{C.}$) and those resulting from the radial variation of α as shown in Figure 3.1. The same three thermal loadings described above were applied. This yielded six additional cases.

3.2 Structural Models

The structural models used in this analysis are the same 60° segment models with equivalent solid cores that are described in Section 2.3. The variation of the thermal coefficient α with temperature for the material CERVIT for use in the analysis of the Itek mirror is shown in Figure 3.2. From that the values of α were derived and used to compute surface displacements. These values of α are given in Table 3.1.

Distribution of "a" in CERVIT Extreme Values*

	10° C. Operation	15° C. Operation	20° C. Operation
Top Face	+6x10 ⁻⁸ M/M-°C	+2.0x10 ⁻⁸ M/M- ^O C	-1.5x10 ⁻⁸ M/M- ^O C
Core	+4x10 ⁻⁸ M/M- ^O C	-1.75x10 ⁻⁸ M/M-°C	-4.0x10 ⁻⁸ M/M ^O C
Bottom Face	+2x10 ⁻⁸ M/M- ^o C	-2.5x10 ⁻⁸ M/M-°C	-4.5x10 ⁻⁸ M/M- ^O C

* Information from NASA/MSFC Memo dated May 2, 1974 See Fig. 3.2

Table 3.1

A typical variation of α in a fabricated ULE lightweight mirror is given in Figure 3.1. Figure 3.3 shows a distribution of α that was used to compute a "worst case" condition for the Perkin-Elmer mirror.

3.3 Results

The peak deflections of the mirror surface, resulting from the 18 loading cases described in Section 3.1, are given in Table 3.2. Additionally, the contours of the deflected mirror surface for each case are shown in Appendix Figures A-3 through A-20.

		Structural Type of	Type of Thermal	Temperature Coefficient	Maximum Deflection, -Z Direction			Fig.
Designer Material		Model	Gradient (OF)	Coefficient	10 ⁻⁹ M or (10 ⁻⁷ in) Peak to Δ Peak *		RMS *	
ITEK	CERVIT	4	1 ⁰ Soak	Nominal	5.33 (2.1)	3.05 (1.2)	.71 (.28)	A3
PERKIN-ELMER	U.L.E.		1 ^O Soak	Nominal	4.50 (1.77)	1.93 (.76)	.38 (.15)	A15
ITEK	CERVIT		1° Soak	10 ^O C Thermal Coefficient	49.02 (19.3)	7.11 (2.8)	1.52 (.60)	А6
ITEK	CERVIT		l ^O Soak	15 ⁰ C Thermal Coefficient	55.88 (22.0)	6.10 (2.4)	1.50 (.59)	A9
ITEK	CERVIT		1 ⁰ Soak	20 ^O C Thermal Coefficient	35.56 (14.0)	3.86 (1.52)	.96 (.38)	A12
PERKIN-ELMER	U.L.E.		1 ^O Soak	Variable	38.61 (15.2)	3.05 (1.2)	1.02	A18
ITEK	CERVIT		l ^O Axial	Nominal	83.82 (33.0)	2.34 (.92)	.41 (.16)	A4
PERKIN-ELMER	U.L.E.		1° Axial	Nominal	51.56 (20.3)	1.14 (.45)	.23 (.09)	λ 16
ITEK	CERVIT	60° segment	l ^o Axial	10 ^O C Thermal Coefficient	47.24 (18.6)	2.41 (.95)	.56 (.22)	A7
ITEK	CERVIT	equivalent solid	1° Axial	15°C Thermal Coefficient	36.07 (14.2)	1.98	.43	A10
ITEK	CERVIT	core	1º Axial	20°C Thermal Coefficient	71.88 (28.3)	2.01 (.791	.46 (.18)	A13
PERKIN-ELMER	U.L.E.		1° Axial	Variable	39.88 (15.7)	2.54 (1.0)	.97 (.38)	A19
ITEK	CERVIT		1º Radial	Nominal	7.11 (2.8)	4.06 (1.6)	.91 (.36)	A5
Perkin-elmer	U.L.E.		1º Radial	Nominal	4.32 (1.7)	2.03	.36 (.14)	A17
ITEK	CERVIT		1° Radial	10 ^O C Thermal Coefficient	28.70 (11.3)	6.86 (2.7)	1.45 (.57)	A8
ITEK	CERVIT	-	1 [°] Radial	15 ^O C Thermal Coefficient	26.42 (10.4)	4.29 (1.69)	.84	A11
ITEK	CERVIT		1° Radíal	20°C Thermal Coefficient	13.2 (5.2)	1.96 (.77)	.43 (.17)	A14
PERKIN-ELMER	U.L.E.		1° Radial	Variable	14.73 (5.8)	1.45 (.57)	.53 (.23)	A20

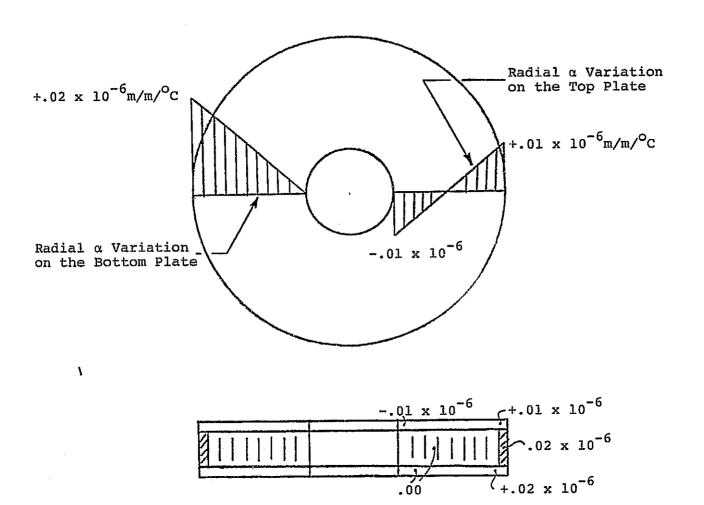
^{*}Peak to Peak and RMS from Best Fit Sphere.

Table 3.2

Maximum Deflections of Itek and Perkin-Elmer Mirror Surfaces Under Thermal Loads

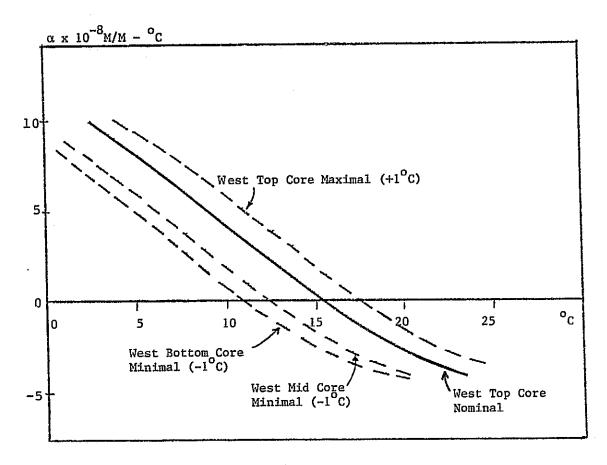
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Data From Corning Visit 26/3/74



Nominal $\alpha = .03 \times 10^{-6} \text{m/m/}^{\circ}\text{C}$

Figure 3.1 Radial Variation of Thermal Expansion Coefficient α , Perkin-Elmer Mirror



CERVIT 101 "a" Variations

Data from May 2/7.4 NASA/MSFC S&E-SSL-PO/TCOR Nominal α : .05 x 10⁻⁶ M/M - $^{\circ}$ C

Figure 3.2 Variation of Thermal Expansion Coefficient $\boldsymbol{\alpha}$ With Temperature

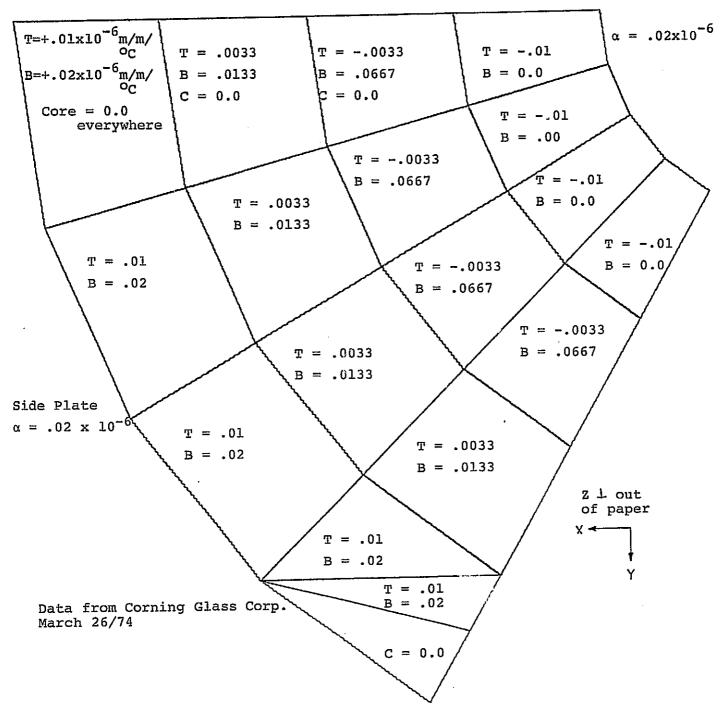


Figure 3.3 Probable Distribution of Thermal Expansion Coefficient of α in U.L.E. Mirror

Chapter 4

STRUCTURAL EVALUATION OF THE BOEING MIRROR LIGHTWEIGHTING CONCEPT

4.1 Description of Mirror Design

The properties of the Boeing mirror that were analyzed are listed in Table 4.1:

.,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	
Outside Diameter	122" (3.099m)
Inside Diameter	23.5" (.597m)
Spherical Radius of Curvature	525" (13.335m)
Radial Thickness	17.38" (.442m)
Cell Shape	Hexagonal
Cell Pitch	4.8" (.122m)
Top Plate Thickness	1.83"(.047m)
Bottom Plate Thickness	1.64" (.042m)
Bottom Plate Hole Diameter	3.25" ø (.083m)
Edge Band Thickness	.40" (.0102m)
Cell Wall Thickness	.20" (.005lm)
Material	CERVIT 101
Total Weight Mirror	4500 lbs. (2045 Kg)

Table 4.1
Properties of Boeing Mirror

The "Boeing" mirror in nearly all ways resembles the Itek mirror. It is machined from a solid blank of CERVIT and has a hexagonally-lightweighted core. It differs from the Itek design in that additional lightweighting has been provided by machining away the inner and outer circumferential edge bands and lightweighting those partial cells from the edge. Thus all cells in the mirror are uniform. This supposedly reduces the cost and risk of normal lightweighting.

During operation the mirror is again held at three cylindrical trunnions, 120° apart, at the mid-height of the outside edge with supports allowing expansion in the radial direction.

4.2 Gravity Load

A gravity load was applied in the direction of the optical axis (-Z direction).

4.3 Structural Model

The structural model was similar to the Itek Phase A "exact" model. That is, both the top and bottom plates and the hexagonally-shaped cells of the core were modeled with plate elements and the support areas with three-dimensional solids. A 60° segment of the mirror, including part of one support on the outside circumference was modeled. Roller supports were provided along the radial edges. The model is shown in Figure 4.1.

4.4 Results

A comparison of the deflection of the Boeing mirror with various other very similar design concepts that were

evaluated in Phase A is shown in Table 4.2. Optical surface deformations are presented in Figure A-21. The tensile stresses in the top plate, the bottom plate and the lightweighted cell webs are shown in Figures 4.2, 4.3 and 4.4.

COMPARISON OF DISPLACEMENTS

	Gravity Load			Thermal Load			
Model	Max	Peak to RMS		1°F Rad.	1 ^O F Axial	1 ^O F Soak	
Exact	818 (322)	754 (297)	168 (66)	8.38 (3.3)	6.10 (24)	4.32 (1.7)	
Alternate Webs	884 (348)	836 (329)	218 (86)	7.62 (3.0)	6.10 (24)	4.32 (1.7)	
Approximate	820 (323)	655 (258)	142 (56)	7.37 (2.9)	8.13 (32)	5.84 (2.3)	
Boeing Concept	909 (358)	1190 (467)	213 (84)				
Units 10 ⁻⁸ M(10 ⁻⁶ in.) Units 10 ⁻⁹ M (10 ⁻⁷ in.						0 ⁻⁷ in.)	

Table 4.2*

^{*} Reference to Phase A results

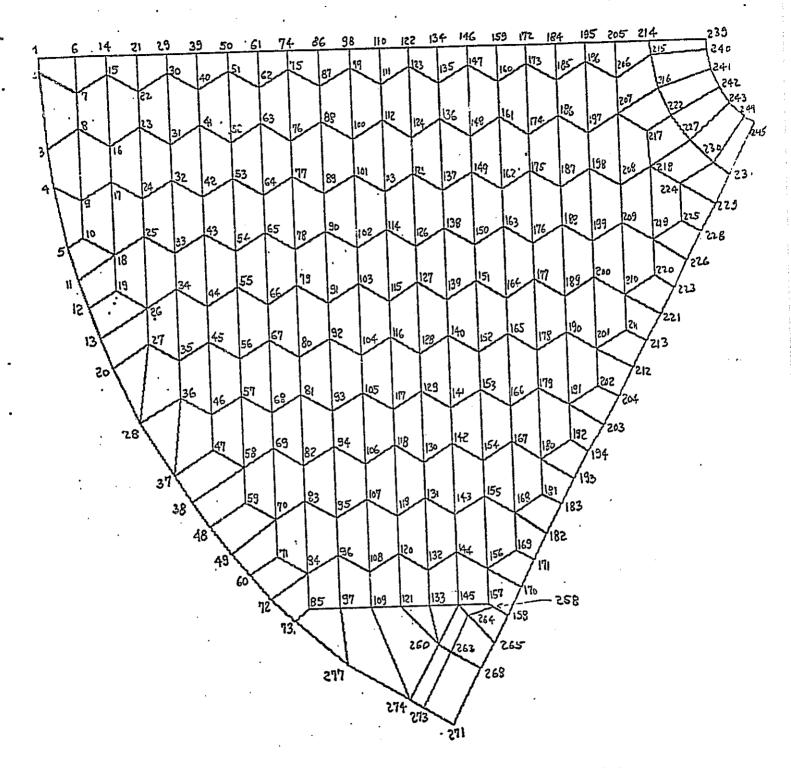


Figure 4.1 Boeing Concept Mirror, Finite Element Model of the Optical Surface

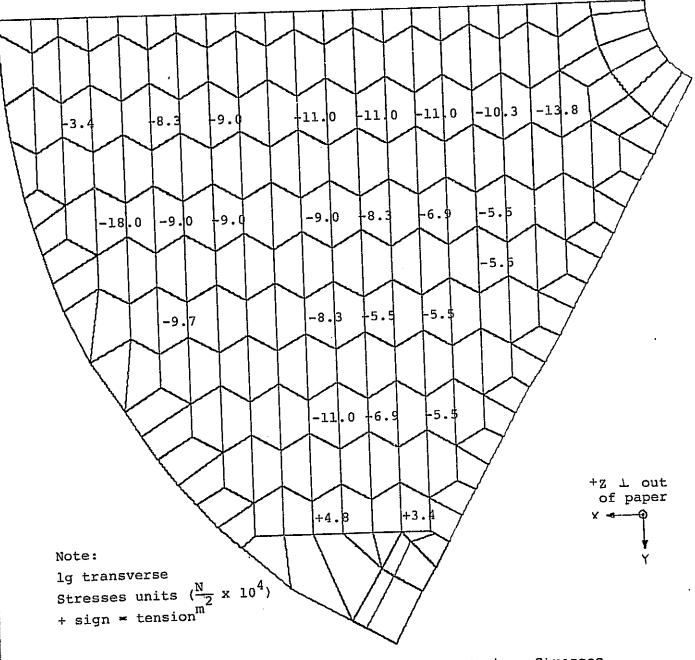


Figure 4.2 Boeing Concept Mirror, Maximum Stresses in the Top Plate

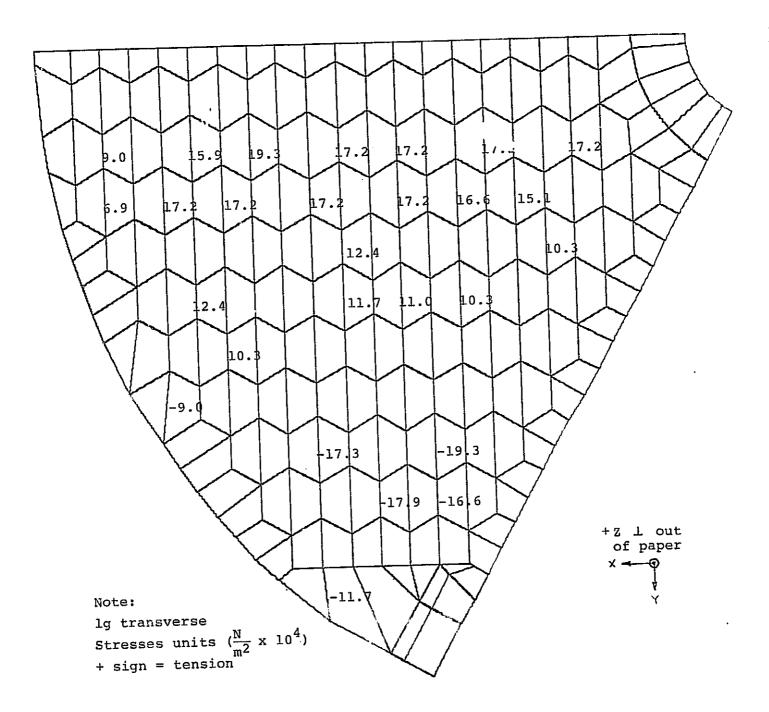


Figure 4.3 Boeing Concept Mirror, Maximum Stresses in the Bottom Plate

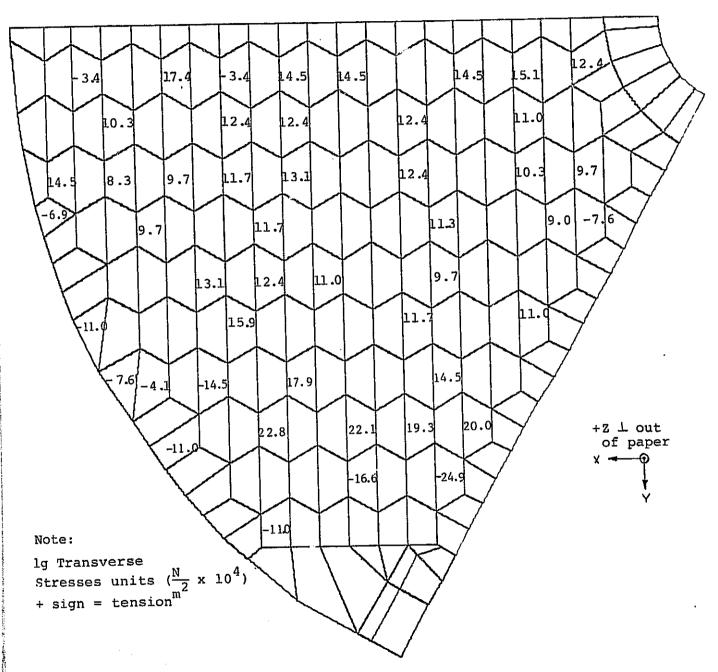


Figure 4.4 Boeing Concept Mirror, Maximum Stresses in the Core Webs

Chapter 5

ADDITIONAL STUDIES

5.1 Study to Determine The Effect of Cell Plate Deflection

The deflection at the center of a hexagonal lightwww uting cell plate relative to the edges has usually been considered to be of second order. In any case the model to evaluate this in one step is likely to be prohibitive in cost. A study was conducted to determine whether the assumption that this deflection is of second order was justifiable.

Using the results of the Itek Phase A exact mirror analysis for the case a 1G load parallel to the optical axis, the nodal deflections at the six corners of each hexagonal cell were averaged at the center. The deflection at the center of a thick hexagonal plate under a 1G load was calculated and added to the averaged deflections, thus obtaining a corrected deformation of the optical surface. The results of the study are shown in Table 5.1.

MODEL	ΜΑΧ Δ	Peak to Peak	RMS	
Itek Phase A "Exact"	813 (320)	754 (297)	168 (66)	
Itek Phase A "Exact" plus Cell Deflection	818 (322)	757 (298)	170 (67)	

NOTE: Units M x 10^{-8} or () IN.X 10^{-6}

Table 5.1
COMPARISON OF DISPLACEMENTS
ITEK PHASE A "EXACT" MIRROR

5.2 Fracture Toughness in CERVIT and ULE

The basic fracture toughness equations for Mode I and Mode II loading are given and comparisons are made between the expected performance of ULE and CERVIT.

In the manufacture of lightweight large optical mirrors, it is likely that there will be regions of separation between the core and the front face plate of the mirror as well as cracks caused by the machining of the material. In order to estimate the critical separation or crack length $(l_{\rm C})$, which could propagate under stress and destroy the mirror, one must consider linear elastic fracture mechanics. For the Mode I fracture mode (Figure 5.1) the specimen is assumed to be in a state of plane stress, with the loading perpendicular to the length of the crack. For a given crack length (c), the crack will propagate when

Some data appears to be available on K_{IC} for ULE and CERVIT but not on K_{IIC} . K_{IC} for ULE is approximately 640 psi $\sqrt[4]{1}$ (Corning data). Since the critical problem seems to be the lack of bonding between the core matrix and front face of the mirror, where there is low normal stress and high shear stress, Mode II fracture will prove particularly critical for ULE. An approximate rule of thumb is that K_{IIC} is twice K_{IC} .

Assuming this relationship for $K_{\mbox{II}_{\mbox{C}}}$ and that the debond surface between center matrix and mirror face experiences only shear stress, the curve in Figure 5.2 was generated.

The probability of failure in a brittle material subjected to a given stress is

$$\phi = 1 - \exp(-A \int_0^{S_D} g(s) ds)$$
 (5.1)

where A = Area of part under stress

S_D = Design stress

q(s) = Flaw density function

g(s) is assumed independent of surface area, but is strongly dependent on surface preparation:

$$g(s) = \frac{1}{a} \frac{d\phi}{ds} (\frac{1}{1-\phi(s)})$$
 (5.2)

Generating $\phi(s)$ and $\frac{d\phi}{ds}$ from Figure 5.3 at S = 5500 psi, one obtains $g(s) = 1.681 \times 10^{-5}$. Assuming a linear relation for g(s) between S = 0 and 5500 psi, one obtains $g(s) = .306 \times 10^{-5}$ for S = 1000 psi. Again using a linear variation for g(s) between 0 and 1000 psi, a probability of failure of .015 is obtained for a design stress of 1000 psi and an area of 10 in. Using S = 200 psi gives $g(s) = .06 \times 10^{-5}$ and $\phi = 6.11 \times 10^{-4}$ for an area of 10 in.

Unfortunately, the paucity of data for CERVIT makes it impossible to extrapolate the g(s) curve back to zero stress. This is needed to generate a probability of failure for CERVIT at a shear stress of either 200 or 1000 psi. Figure 5.4 is enclosed to illustrate this.

It is recommended that four point bend tests be run for both ULE and CERVIT, but in particular for CERVIT, to generate the flaw density curve (g(s)) around 1000 psi. Much larger samples (> 10 in. 2) should be tested to determine this part of the curve. Also, $K_{\mbox{II}}$ tests for both CERVIT and ULE should be done.

5.3 Flexibility Matrices for the Itek and Perkin-Elmer Mirror for Use in The Study of Active Figure Control The flexibility matrix is defined by

$$\{u\} = [c] \{p\}$$
 (5.3)

where

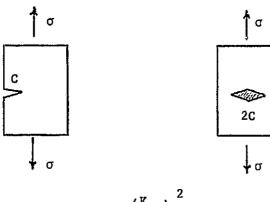
C_{ij} = Flexibility matrix

P_j = Forces vector

 $u_i = Displacement vector$

The flexibility matrix defines a displacement at i due to a unit load at j. Flexibility matrices for both the Itek and Perkin-Elmer mirrors were obtained by applying unit loads parallel to the optical axis (+Z direction) at each node on the back surface of the mirrors. The finite element models that were used were the 360° structural models described in Section 2.3. The flexibility matrices are given in Appendix B.

Mode I Loading

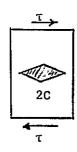


$$c_{C} = \frac{1}{\pi} \left(\frac{K_{I_{C}}}{\sigma} \right)^{2}$$

CERVIT: $K_{I_C} = 850 psi \sqrt{in}$.

ULE: $K_{\underline{I}_C} = 640 \text{psi } \sqrt{\text{in}}$.

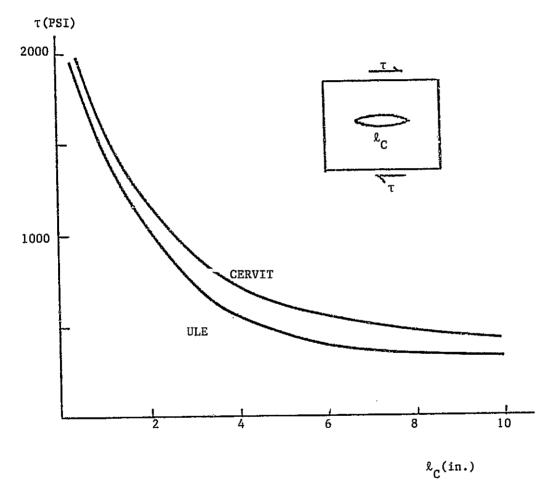
Mode II Loading



"Rule of Thumb"

$$K_{II_C} = 2 \times K_{I_C}$$

$$c_c = \frac{1}{\pi} \left(\frac{K_{II_C}}{\tau} \right)^2$$



Applied Shear Loading (τ) and Critical Crack Length (Debond) ($^{\kappa}_{C}$)

In Current Design $\tau \approx 200 PSI$

 $\ell_{\rm C} \approx 10$ "

Figure 5.2 Applied Shear Loading vs Critical Crack Length

Figure 5.3 Fracture Probability of ULE Corning 7971, Abraded

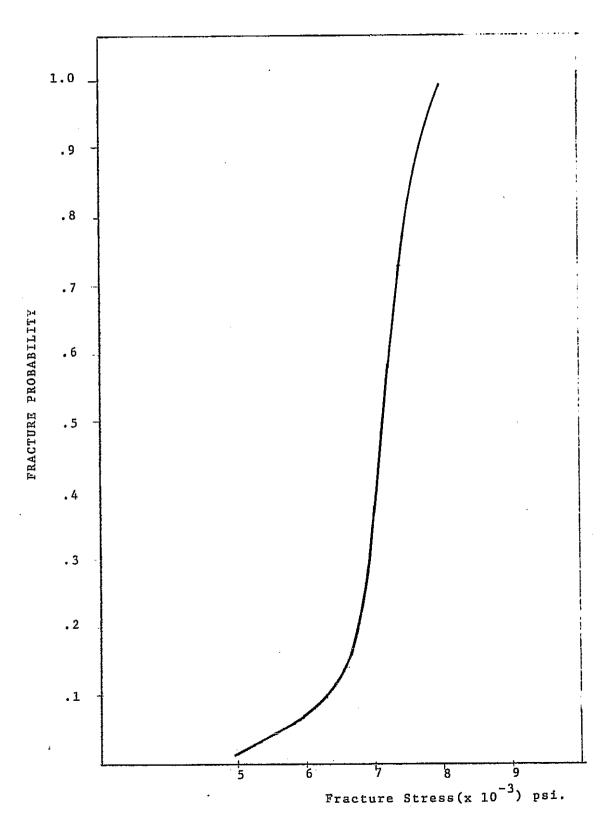
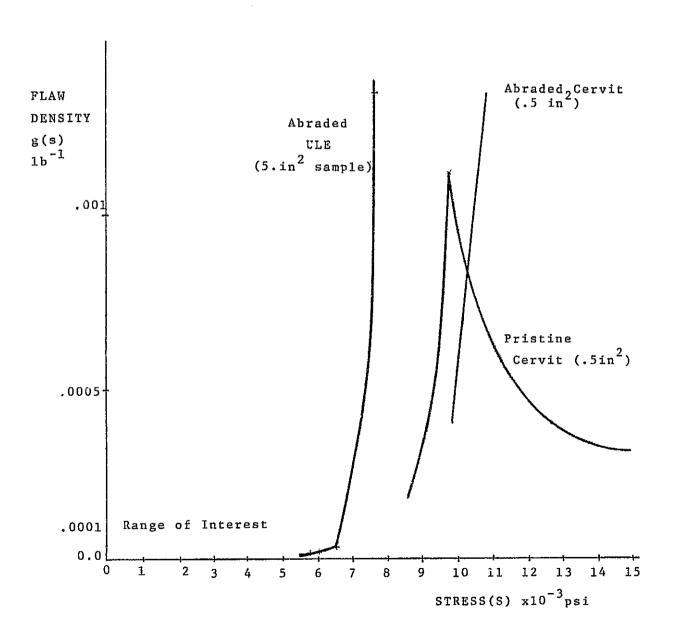


Figure 5.4 Flaw Density vs Stress



CHAPTER 6

SUMMARY, CONCLUSIONS AND RECOMMENDATIONS

A summary of the findings of this investigation is as follows:

- Of the two mirrors, the CERVIT mirror is heavier by about 7%.
- 2. The CERVIT mirror, mainly because of its 35% higher modulus of elasticity, is stiffer with respect to unit transverse inertial loads.
- 3. The stresses in the ULE mirror are less under unit transverse inertial loads.
- 4. Using nominal as well as "real" thermal expansion coefficients, the ULE mirror generally experiences smaller distortions under unit thermal loads.

It is tempting to ask the following question, "Which mirror performs better?" It is not a question that has a realistic answer, however, given the bounds of this study. If the mirrors had been designed to absolutely the same dimensional and mechanical specifications, and then subjected to the same operational environments, then a statement could be made. Otherwise, it is only reasonable to compare the relative performance of the overall systems, of which the primary mirror is one component. If that is not feasible, then a measure of merit could be the performance of the mirror relative to the error budget allocated to it by the optical systems engineering.

It must be remembered that these mirrors are components of two highly complex and substantially different astronomical telescope satellite systems, and in each case the mirror has been designed to fulfill the needs of quite separate concepts of optical systems engineering. For those reasons, the curvatures of these mirrors differ slightly, the central hole size is different, and the thermal and mechanical environments that each experiences will be determined by system parameters not included in this analysis. These considerations have substantially greater impact on the mirror performance than the differences between the ULE and CERVIT designs determined here.

The recommendations that will be made here refer mainly to the reliability of the performance predictions. To date there has been no significant comparison of measured and predicted mirror displacement and stress performance for either a CERVIT or ULE mirror. This is of vital importance since some unknowns still exist in the modelling. In the ULE mirrors this includes the degree of fusion of ribs to flanges, the dimensions after slump, and the effects of posts and holes in the webs. With CERVIT the uncertainties include the stiffening effects of fillets, "wedge" and the rather variable nature of the thermal expansion coefficient.

The paucity of fracture mechanics data for either CERVIT or ULE makes it impossible to assign tensile working stress values. It is highly recommended that additional tests with appropriately sized samples be performed.

APPENDIX A

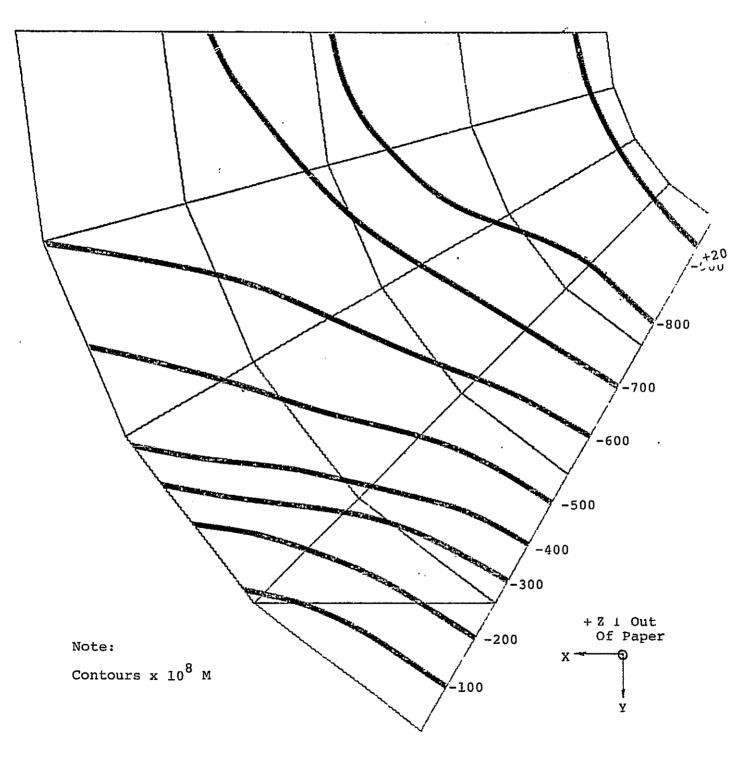


Figure A.1 Z-Deflection Contours of the Itek Mirror Optical Surface, 1G Load (-Z Direction)

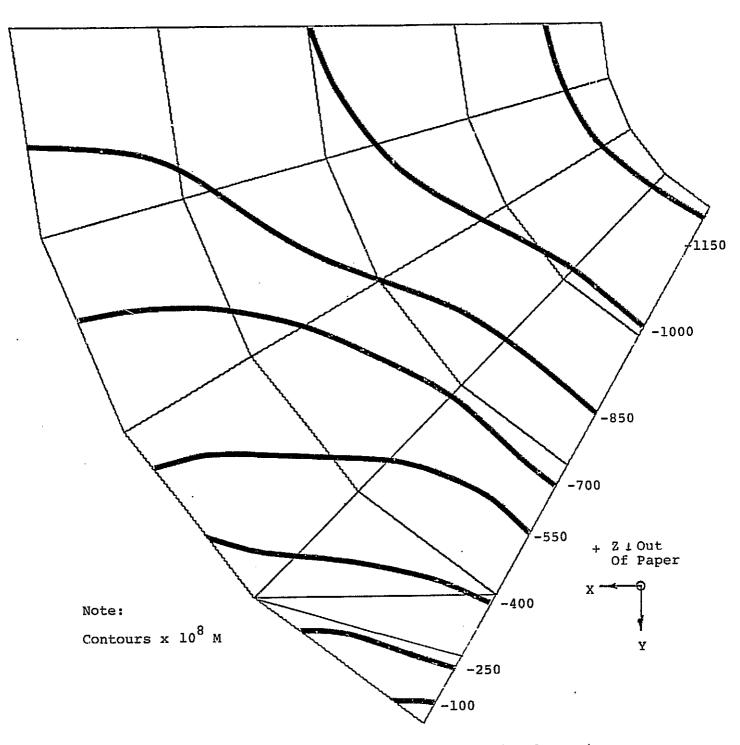


Figure A.2 Z-Deflection Contours of the Perkin-Elmer Mirror Optical Surface, 1G Load (-Z Direction)

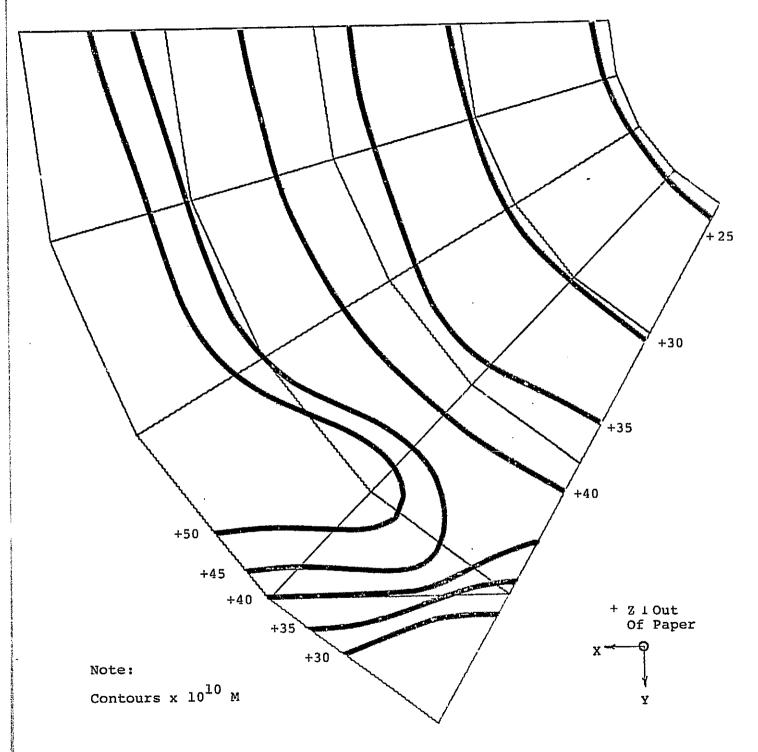


Figure A.3 Z-Deflection Contours of the Itek Mirror Optical Surface, 1°F Soak, Nominal Thermal Coefficient

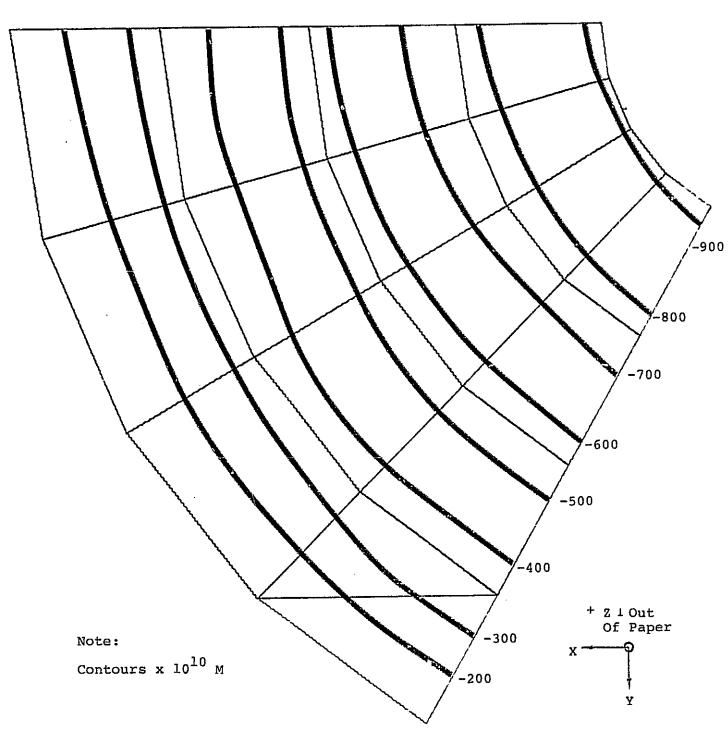


Figure A.4 Z-Deflection Contours of the Itek Mirror Optical Surface, 1°F Axial Gradient, Nominal Thermal Coefficient

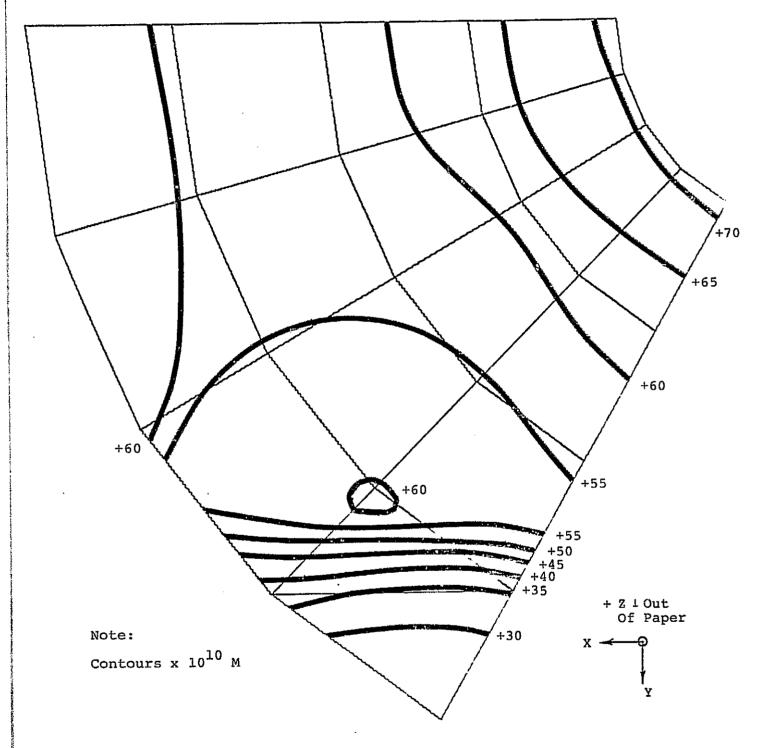


Figure A.5 Z-Deflection Contours of the Itek Mirror Optical Surface, 1 F Radial Gradient, Nominal Thermal Coefficient

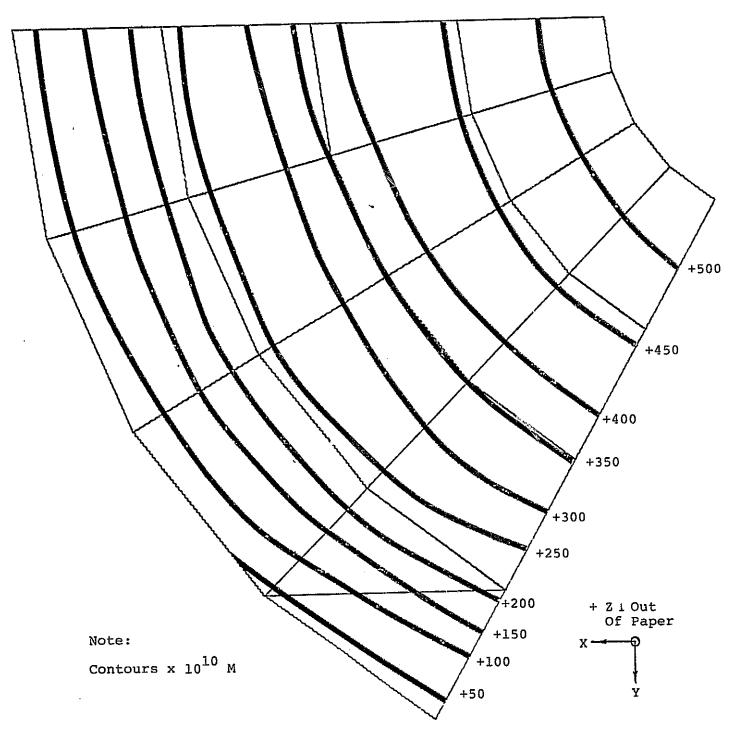


Figure A.6 Z-Deflection Contours of the Itek Mirror Optical Surface, 1°F Soak, Thermal Coefficient @ 10°C

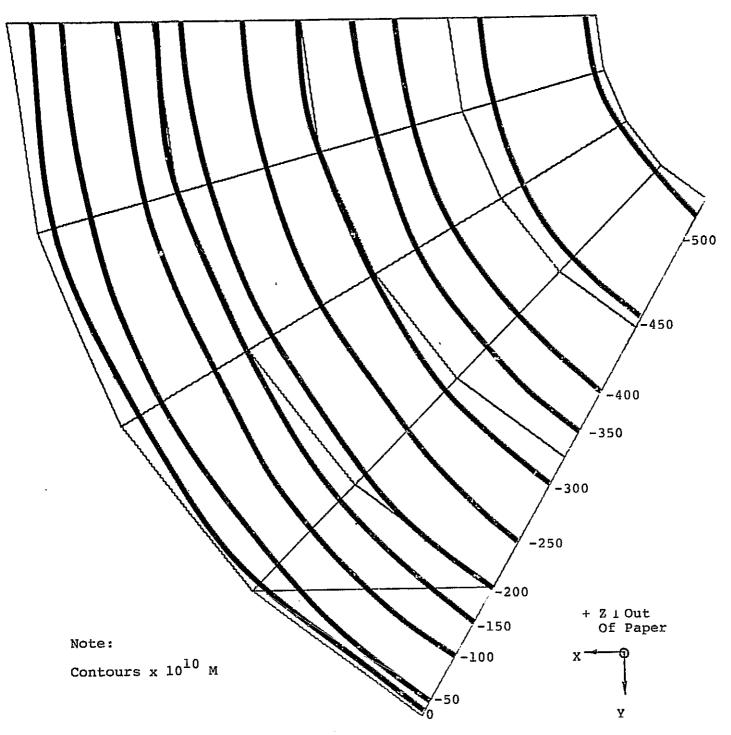


Figure A.7 Z-Deflection Contours of the Itek Mirror Optical Surface, 1°F Axial Gradient, Thermal Coefficient @ 10°C

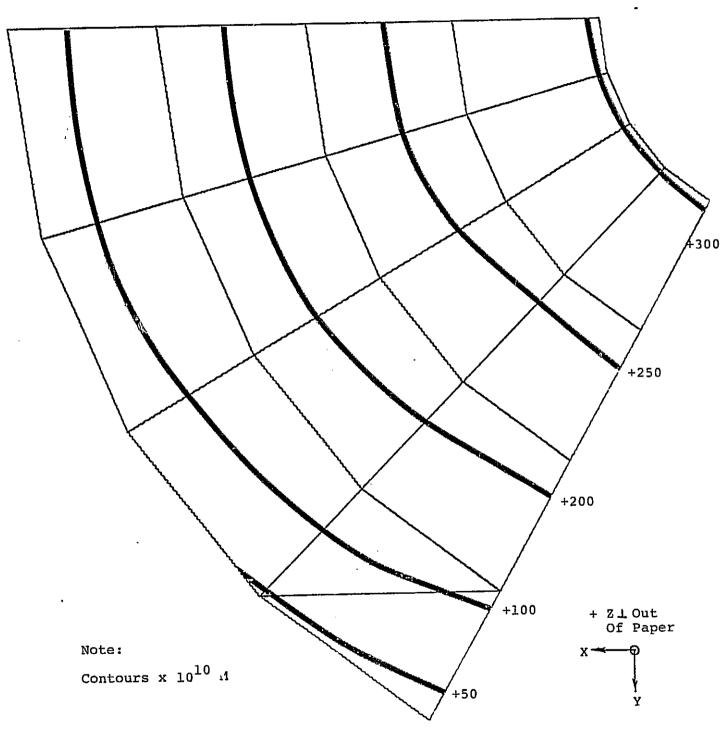


Figure A.8 Z-Deflection Contours of the Itek Mirror Optical Surface, 1°F Radial Gradient, Thermal Coefficient at 10°C

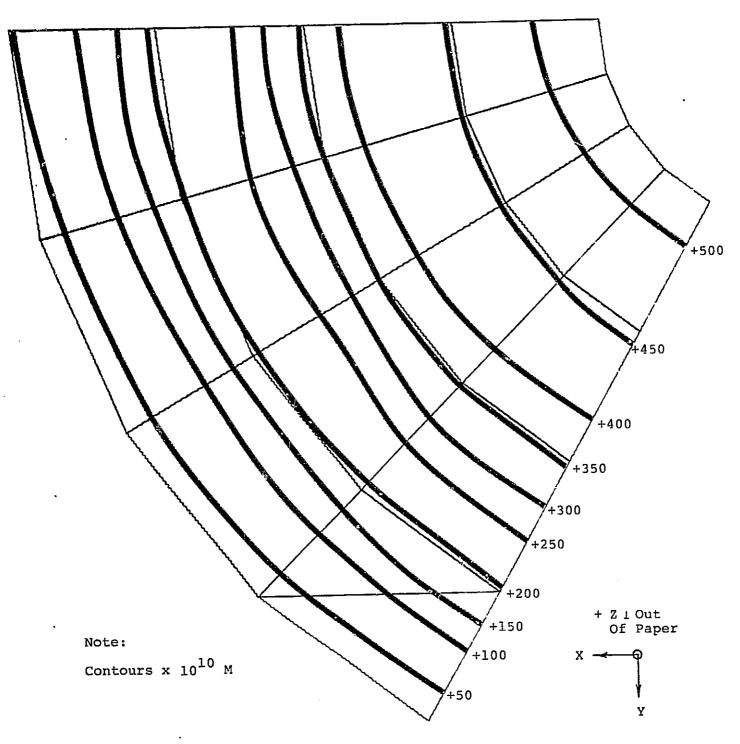


Figure A.9 Z-Deflection Contours of the Itek Mirror Optical Surface, $1^{\rm O}{\rm F}$ Soak, Thermal Coefficient @ $15^{\rm O}{\rm C}$

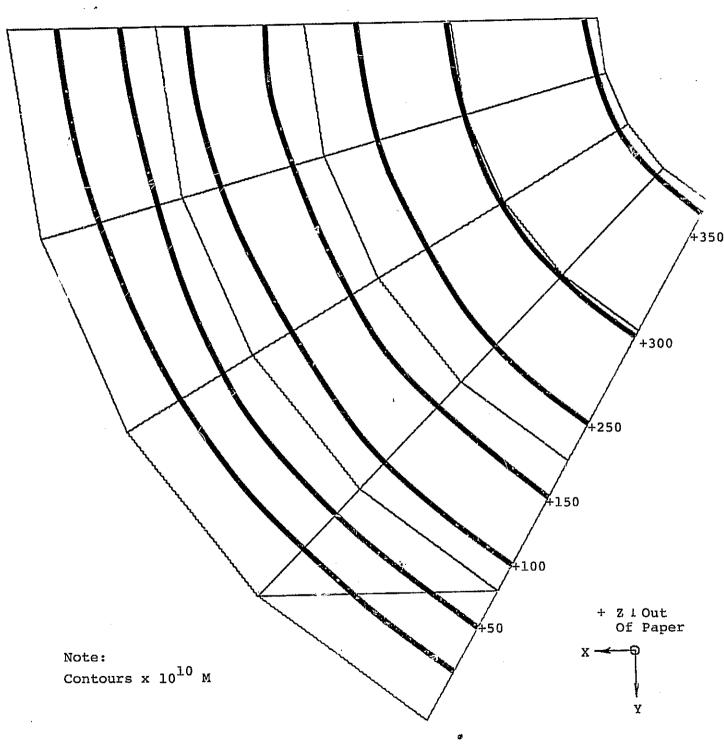


Figure A.10 Z-Deflection Contours of the Itek Mirror Optical Surface, 1 F Axial Gradient, Thermal Coefficient @ 15°C

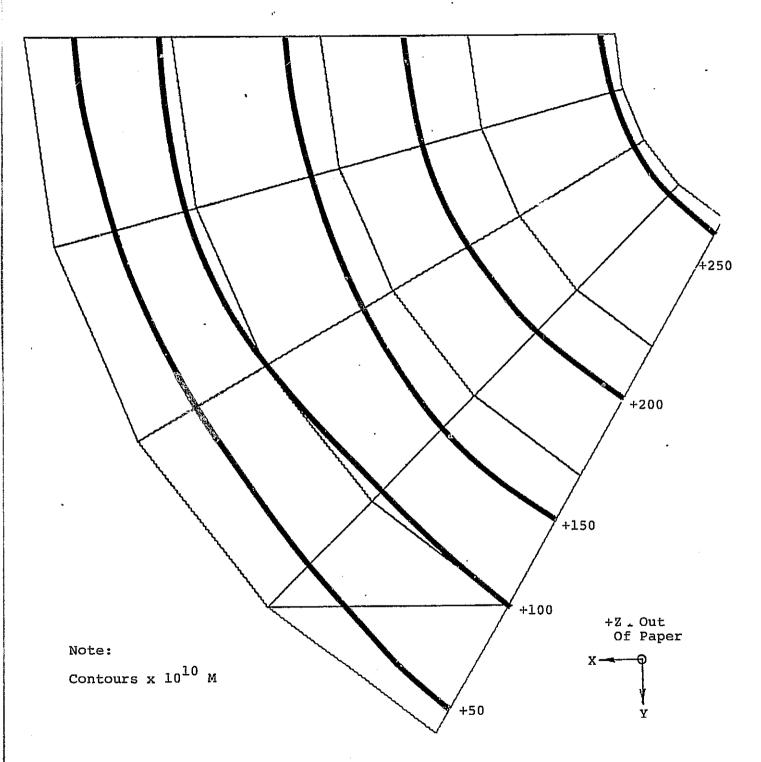


Figure A.ll Z-Deflection Contours of the Itek Mirror Optical Surface, 1 OF Radial Gradient, Thermal Coefficient @ 15 OC

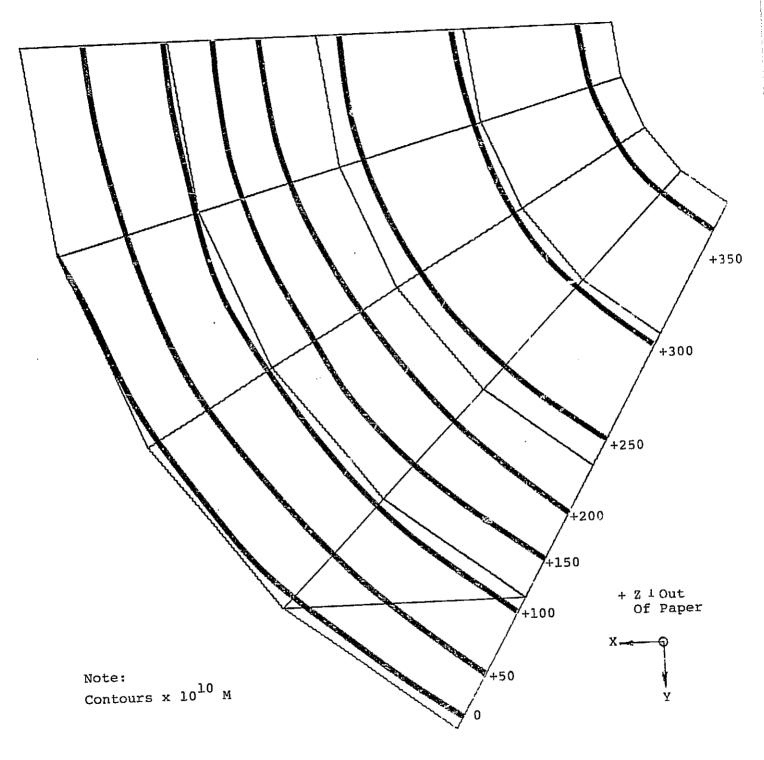


Figure A.12 Z-Deflection Contours of the Itek Mirror Optical Surface, 1°F Soak, Thermal Coefficient @ 20°C

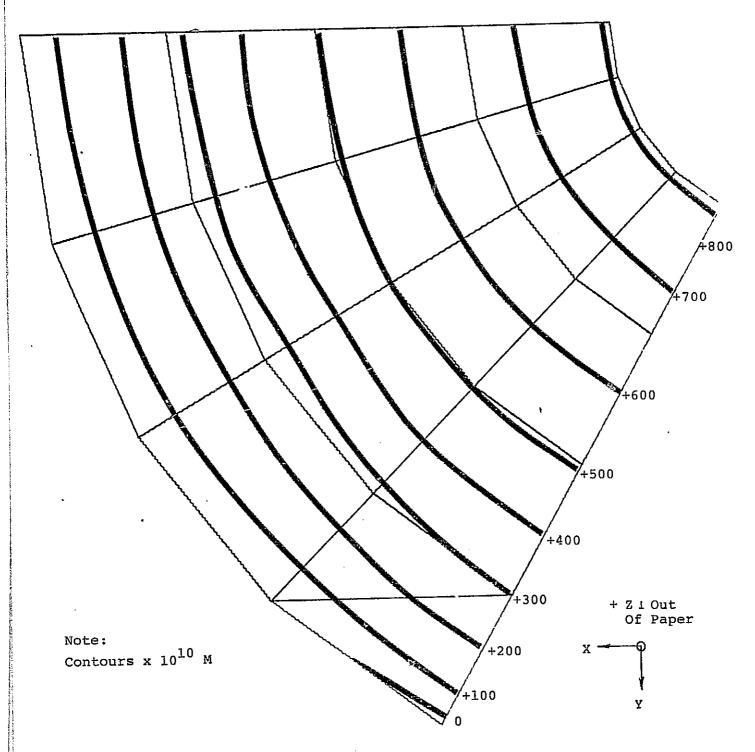


Figure A.13 Z-Deflection Contours of the Itek Mirror Optical Surface, 1°F Axial Gradient, Thermal Coefficient @ 20°C

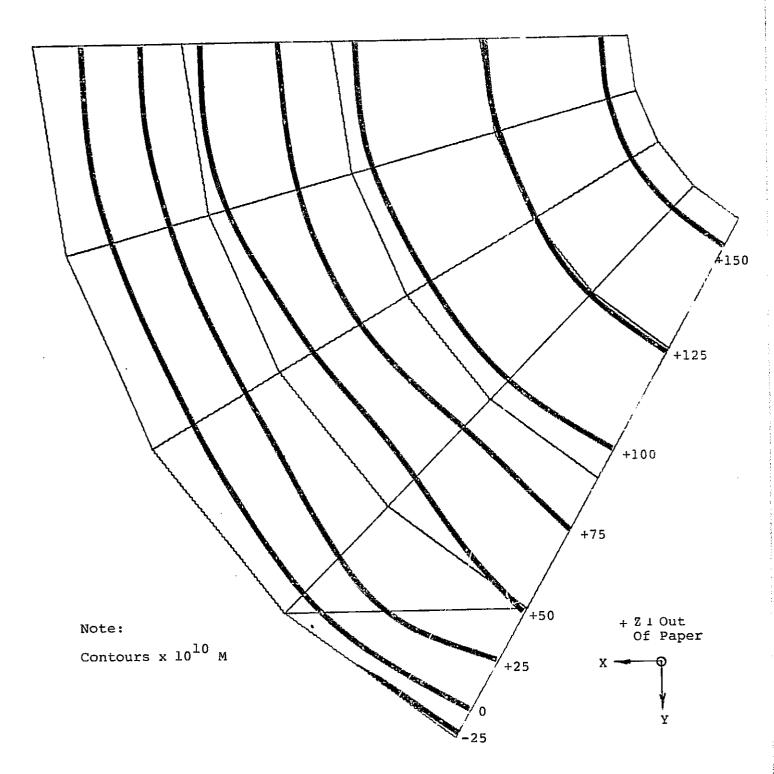


Figure A.14 Z-Deflection Contours of the Itek Mirror Optical Surface, 1 F Radial Gradient, Thermal Coefficient @ 20°C

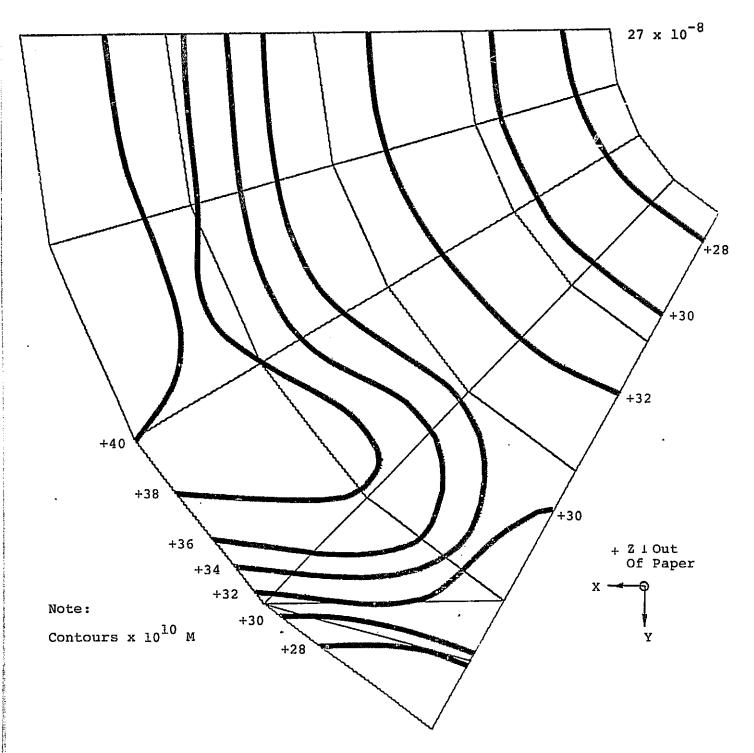


Figure A.15 Z-Deflection Contours of the Perkin-Elmer Mirror Optical Surface, 1 F Soak, Nominal Thermal Coefficient

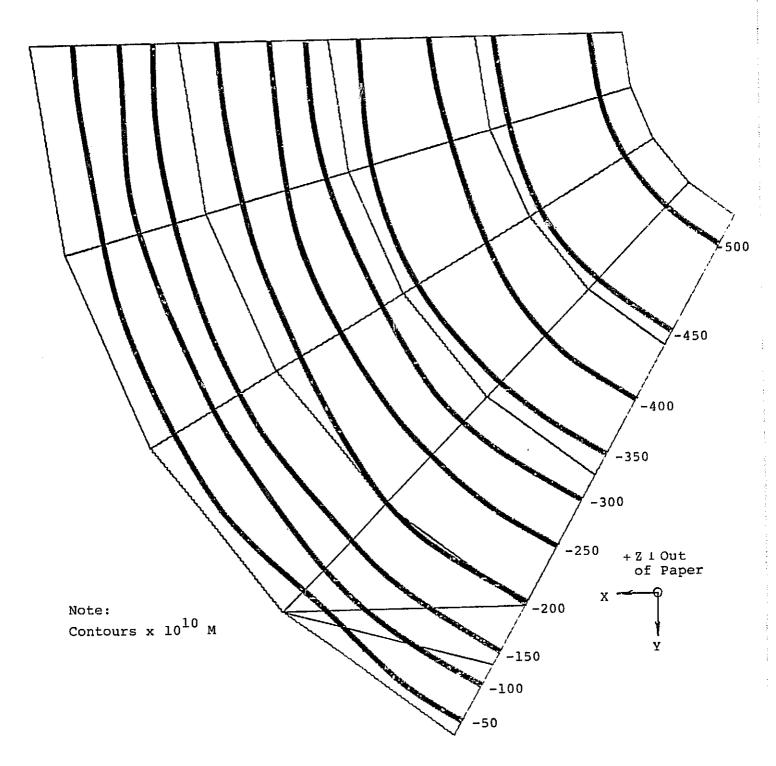


Figure A.16 Z-Deflection Contours of the Perkin-Elmer Mirror Optical Surface, 1°F Axial Gradient, Nominal Thermal Coefficient

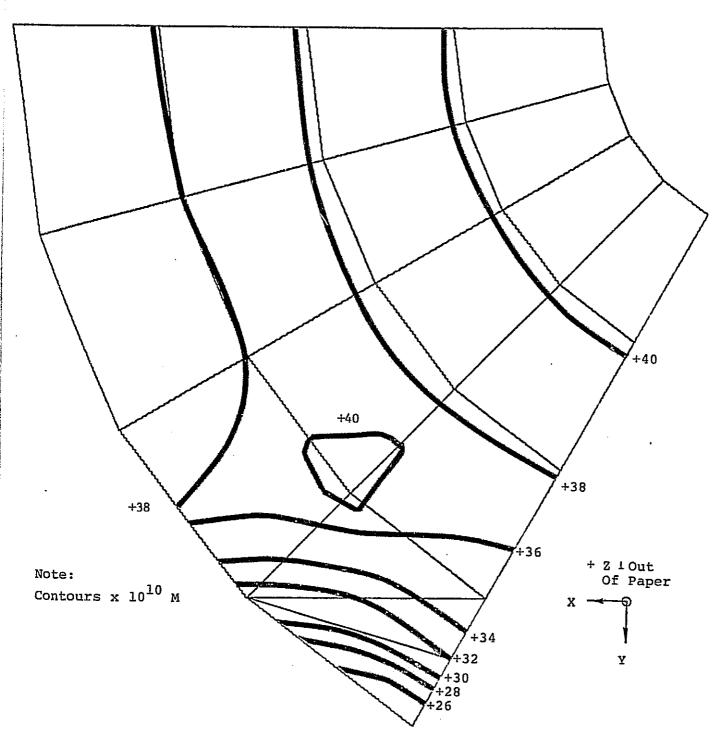


Figure A.17 Z-Deflection Contours of the Perkin-Elmer Mirror Optical Surface, 1 F Radial Gradient, Nominal Thermal Coefficient

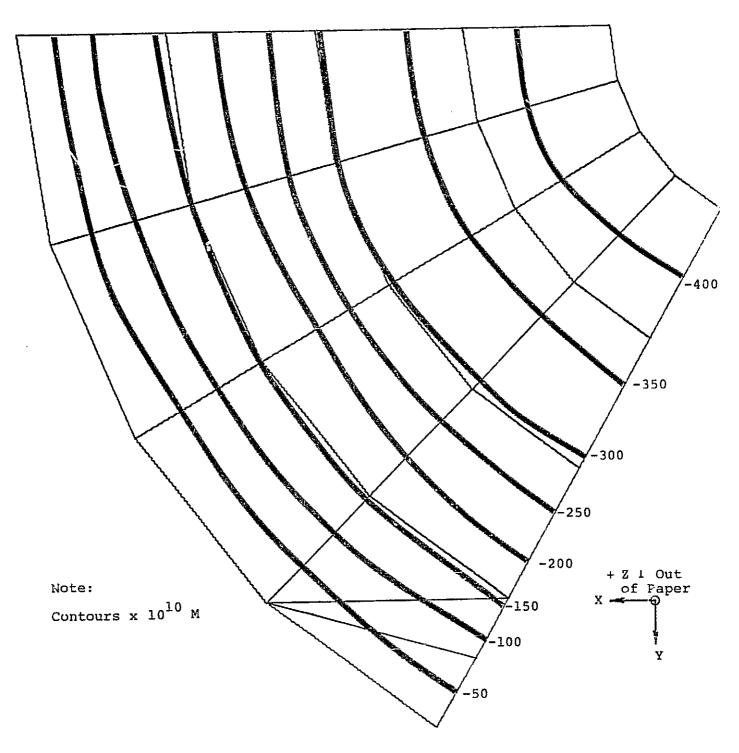


Figure A.18 Z-Deflection Contours of the Perkin-Elmer Mirror Optical Surface, 1°F Soak, Variable Thermal Coefficient

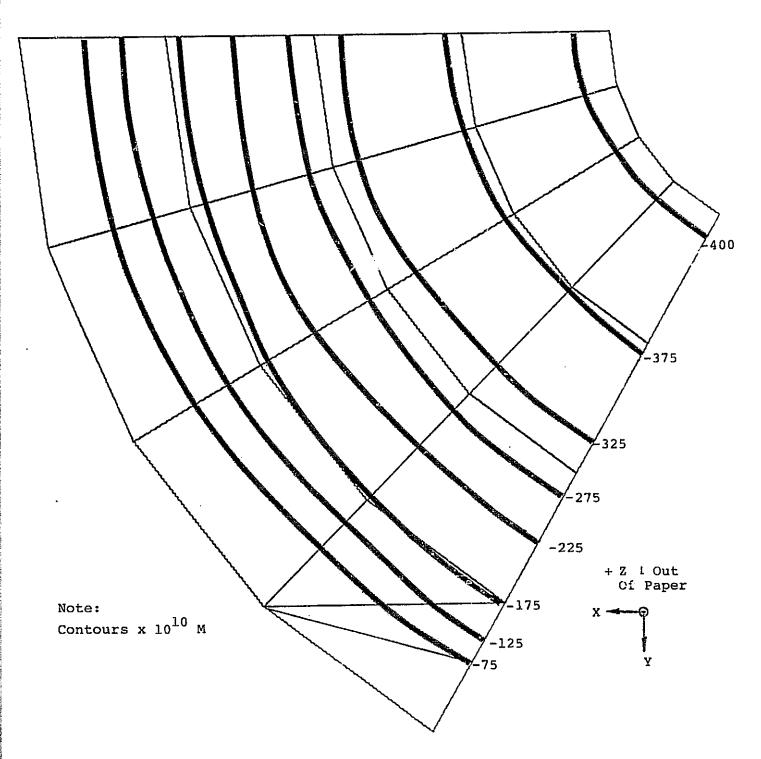


Figure A.19 Z-Deflection Contours of the Perkin-Elmer Mirror Optical Surface, 1°F Axial Gradient, Variable Thermal Coefficient

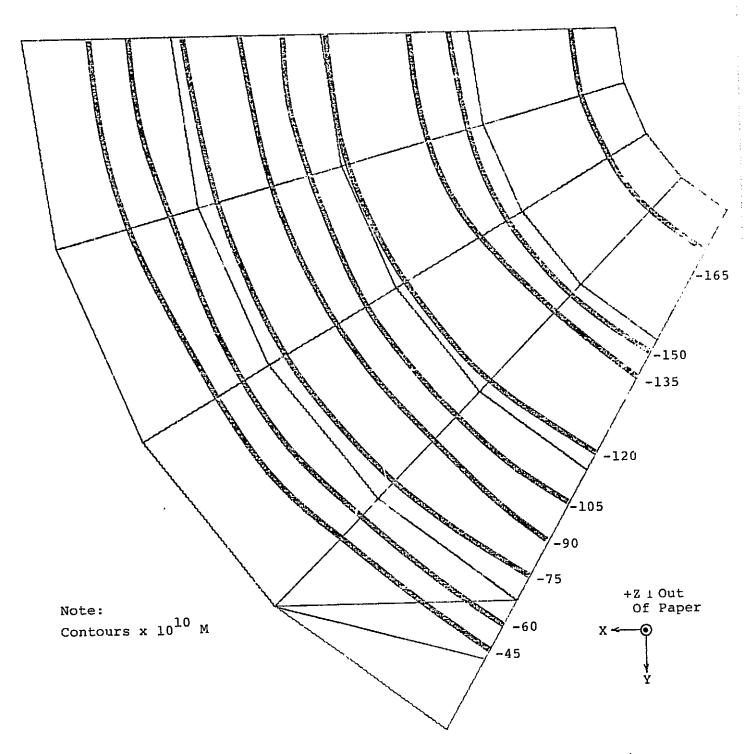


Figure A.20 Z-Deflection Contours of the Perkin-Elmer Mirror Optical Surface, 1 F Radial Gradient, Variable Thermal Coefficient

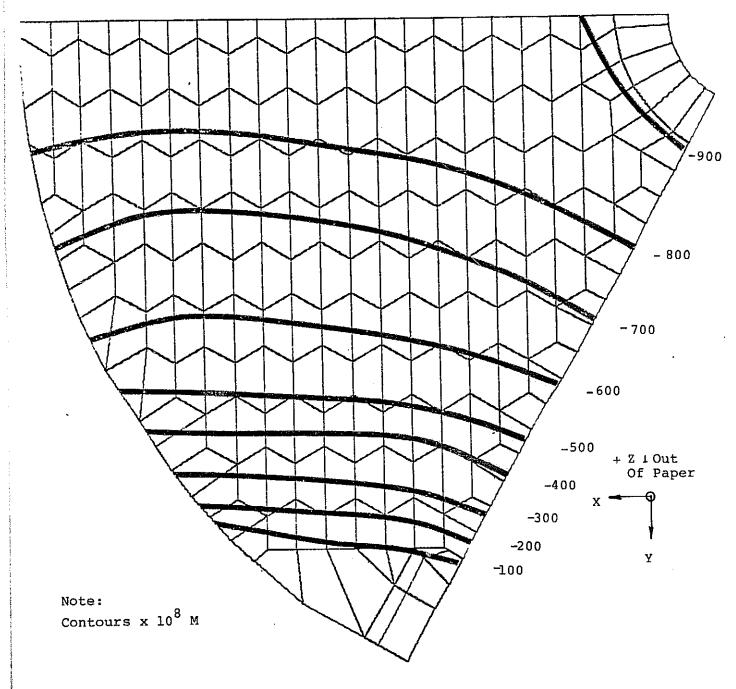


Figure A.21 Z-Deflection Contours of the Boeing Mirror Optical Surface, lg Transverse (-Z Direction)

APPENDIX B

The flexibility matrices of the Itek and Perkin-Elmer mirrors have been computed and are listed below. Refer to Figures 2.3 and 2.4 for topology and joint numbering.

While it is of interest to know the mirror displacements everywhere on the reflecting surface, it is not possible to place actuators at all locations on the back (Note that with these thick mirrors, the concept of a neutral surface as in a plate or shell does not apply.) Thus actuator positions are not considered at the inner and outer peripheries of the mirror, or at the immediate support locations. Therefore, displacements are obtained at 120 nodes, but actuators are located at 69 nodes.

The listing on the following pages have nine columns in three groups of three. In each group:

1st column is the displacement location 2nd column is the actuator location 3rd column is the element of the flexibility matrix

The magnitude of the flexibility elements are:

- to get inches/pound multiply element listed by 10⁻⁶ a.
- to get meters/Newton multiply element listed by b. 5.71×10^{-9}

Both flexibility matrices (Itek and Perkin-Elmer) are also available in form of punched cards and may be obtained upon request from Charles Stark Draper Lab., Inc., in Cambridge, Massachusetts 02139.

OF THE ITEK MIRROR

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   12
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                                                   1
                                 0.447980E
                                             00
                             18
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                                                       27
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                             24
        0.269392E 00
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                                                         -0.914114E-01
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                                 0.174511E
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                             29
        0.118239E 00
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   28
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                                                       37 -0.158778E 00
                                 0.939088E-01
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                             34
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                                  0.473270E-02
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                                -0.934623E-01
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                             67
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ternament in transportung dan dari ternamen generatur di berikan per dakan per terbagai berikan dan beratar b

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Application of a group of the control of the control

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and the state of the contract of the contract

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amentaly and produce that is produced as a filter to the relational constants with the constant and the safety

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                              87
                                   0.184502E 00 119
                                                       88
                                                           0.236311E 00
119
      84
          0.258295E 00 119
                                                           0.277922E 00
                                                       93
          0.286406E 00 119
                              92
                                   0.224670E 00 119
119
      89
          0.321224E 00 119
                              97
                                   0.283949E 00 119
                                                       98
                                                           0.332008E
                                                                      00
119
      94
      99
          0.362236E 00 119 103
                                   0.396774E 00 119
                                                     104
                                                           0.407254E
                                                                      00
119
          0.471559E 00 119 108
                                   0.464041E 00 119 109
                                                           0.452739E 00
119 107
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119	112	0.542838E	00	119	113	0.516706E	00	119	114	0.501353E	00
119	117	0.568759E	00	119	118	0.546237E	00	119	119	0.492664E	00
120	2	0.402988E	00	120	3	0.412956E	00	120	4	0,439687E	00
120	7	0.366310E	00	120	Я	0.388405E	00	120	9	0.421595E	00
120	12	0.311716E	00	120	13	0.353769E	00	120	14	0.395889E	00
120	17	0.258568E	00	120	18	0.319085E	00	120	19	0.369066E	00
120	23	0.291715E	00	120	24	0.344580E	00	120	27	0.221335E	00
120	28	0.272494E	00	120	29	0.323909E	00	120	32	0.212872E	0.0
120	33	0.258595F	00	120	34	0.306985E	00	120	37	0.203364E	00
120	38	0.246153E	0.0	120	39	0.293179E	00	120	42	0.192073E	00
120	43	0.235250E		120	44	0.282692E	00	120	47	0.176027E	00
120	48	0.223120E	0.0	1.20	49	0.273567E	00	120	52	0.159429E	0.0
120	53	0.213601E	00	120	54	0.267509E	00	120	57	0.149638E	00
120	58	0.209424E	0.0	120	59	0.265257E	00	120	63	0.212602E	0.0
120	64	0.267207E	00	120	67	0.172776E	00	120	68	0.221769E	00
120	69	0.273096E	0.0	120	72	0.190429E	00	120	73	0.234390E	00
120	74	0.282234E	00	120	77	0.206112E	00	120	78	0.247849E	00
120	79	0.293995E	00	120	82	0.219204E	00	120	83	0.2617675	0.0
120	84	0.308149E		120	87	0.228878E	00	120	88	0.275761E	
120		0.324788E		120	92	0.237983E	0.0	120	93	0.293562E	
120		0.344821E	00	120	97	0.258131E	00	120	98	0.3184218	
120		0.368474E	0.0	120	103	0.350694E	00	120	104	0.394550E	00
120		0.357387E	0.0	120	108	0.384265E	00		109	0.419867E	
120		0.3968246		120	113	0.409611E	00	120	114	0.438033E	
120	_	0.413582E		120	118	0.417210E	00	120	119	0.454440E	00
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